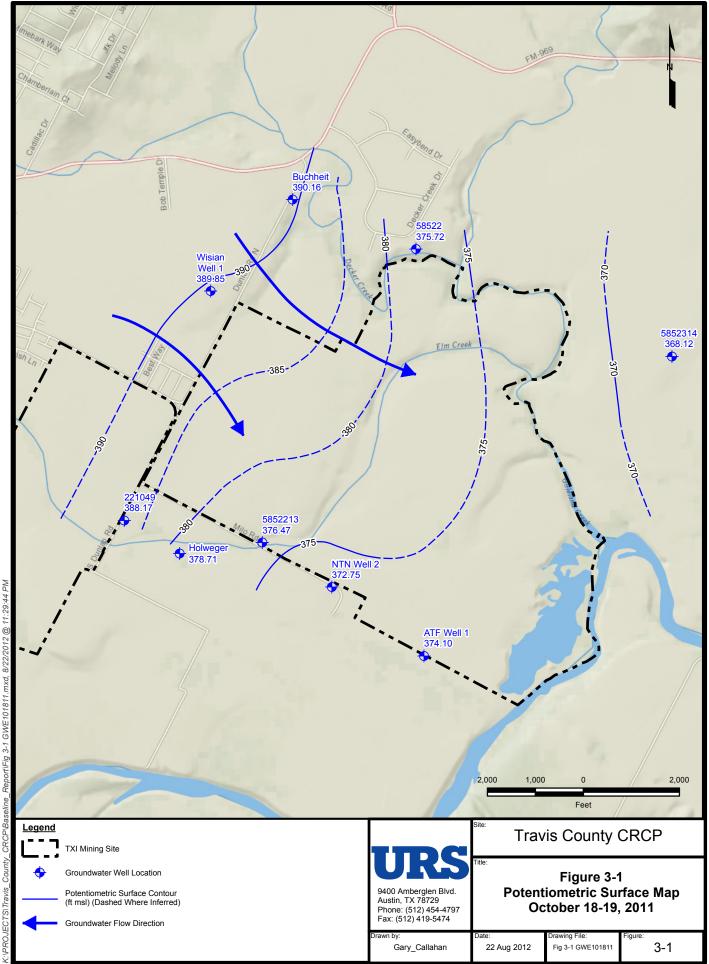
Sampling		Nort	h Site	Sout	th Site
Event	Date	PM ₁₀ (μg/m ³)	PM _{2.5} (μg/m ³)	PM ₁₀ (μg/m ³)	PM _{2.5} (μg/m ³)
1	10/20/2011	28.1	7.6	15.8	7.5
1	10/23/2011	24.9	10.7	19.9	10.7
1	10/26/2011	11.9	8.1	15.0	8.2
1	10/29/2011	27.5	9.0	22.1	10.3
1	11/1/2011	22.6	11.7	28.6	13.6
1	11/4/2011	15.4	6.7	NV-L	7.4
2	1/5/2012	21.9	4.0	24.6	10.8
2	1/8/2012	31.7	10.3	31.9	19.3
2	1/11/2012	11.8	NS	12.5	6.5
2	1/14/2012	33.2	NS	17.5	8.9
2	1/17/2012	13.6	NS	13.9	NS^1
2	1/20/2012	21.5	NS	60.1	16.0
3	3/15/2012	14.7	10.0	NS	9.0
3	3/18/2012	12.9	7.8	NS	10.3
3	3/21/2012	13.8	5.7	NS	5.8
3	3/24/2012	16.5	12.5	NS	11.7
3	3/27/2012	18.1	10.6	NS	NV-C
3	3/30/2012	19.6	13.3	NS	12.2
4	5/3/2012	16.5	NV-L	22.4	NS
4	5/6/2012	14.7	NV-L	22.8	NS
4	5/9/2012	19.7	12.5	32.9	NS
4	5/12/2012	11.3	9.2	16.7	NS
4	5/15/2012	17.2	8.5	27.9	NS
4	5/18/2012	18.1	NV-L	22.2	NS
	Average	19.1	9.3	23.9	10.5

Table 3-3. Air Quality PM_{2.5} and PM₁₀ Size Fraction Results

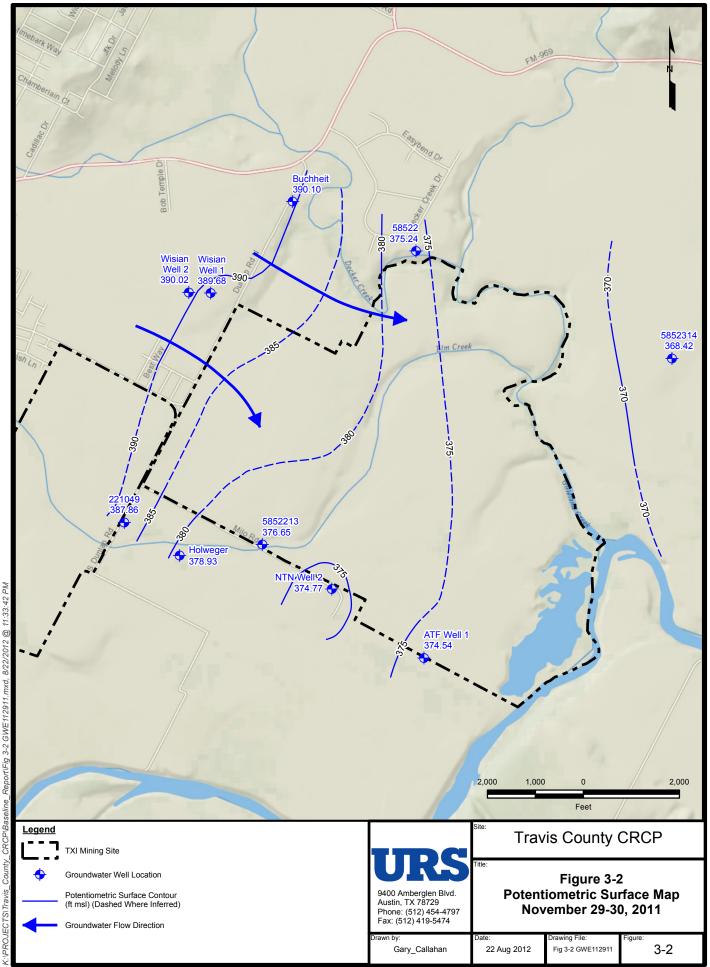
μg/m³ - Micrograms per cubic meter. NS - Not sampled due to faulty air pump. NS¹ - Not sample due to faulty wire. NV-C - Sample not valid due to filter contamination. NV-L - Sample not valid due to low value.

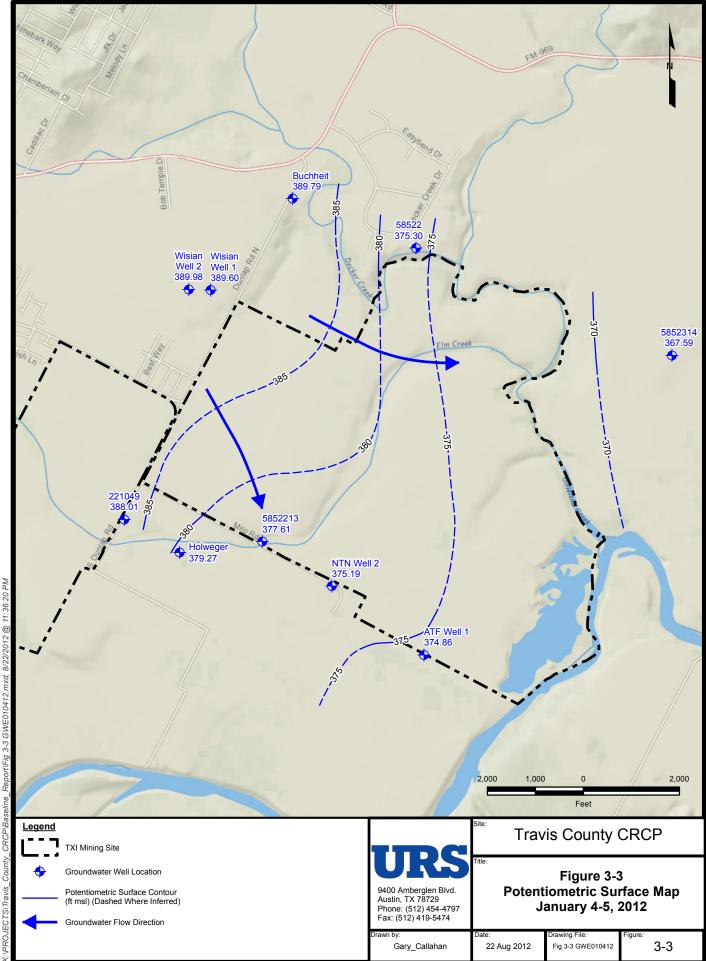
 PM_{10} - Particulate matter less than 10 microns in diameter.

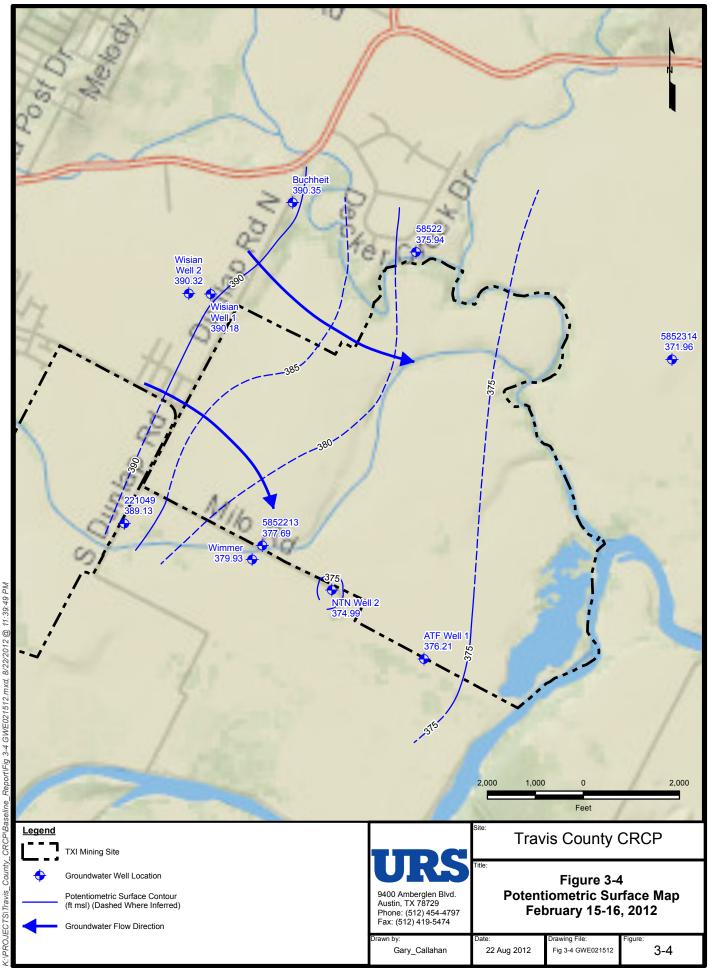
 PM_{25} - Particulate matter less than 2.5 microns in diameter.

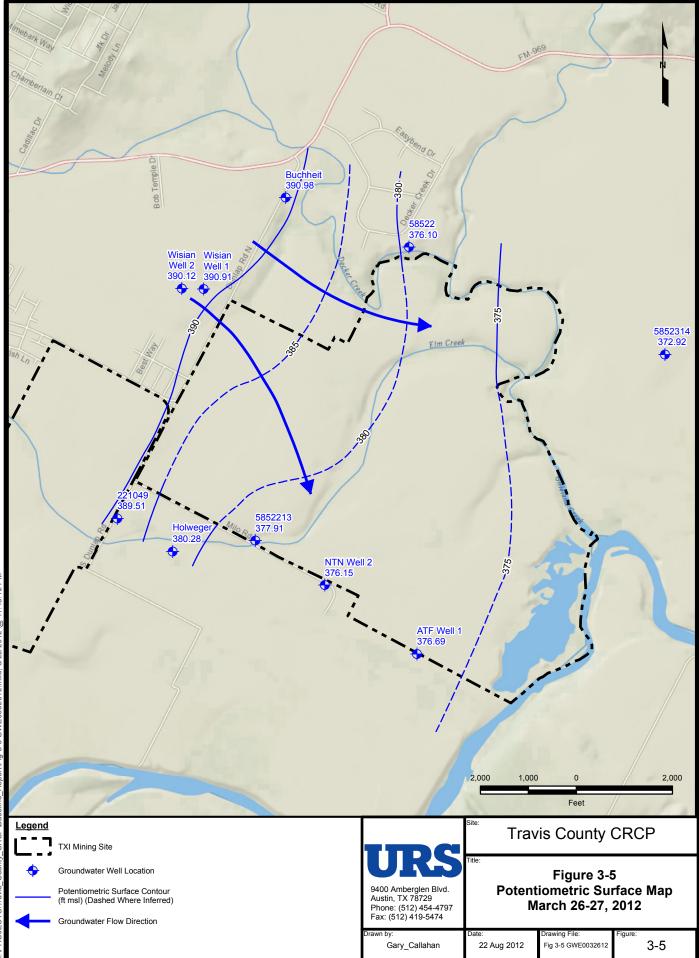


Baseline Report - Environmental Monitoring CRCP Travis County, Texas



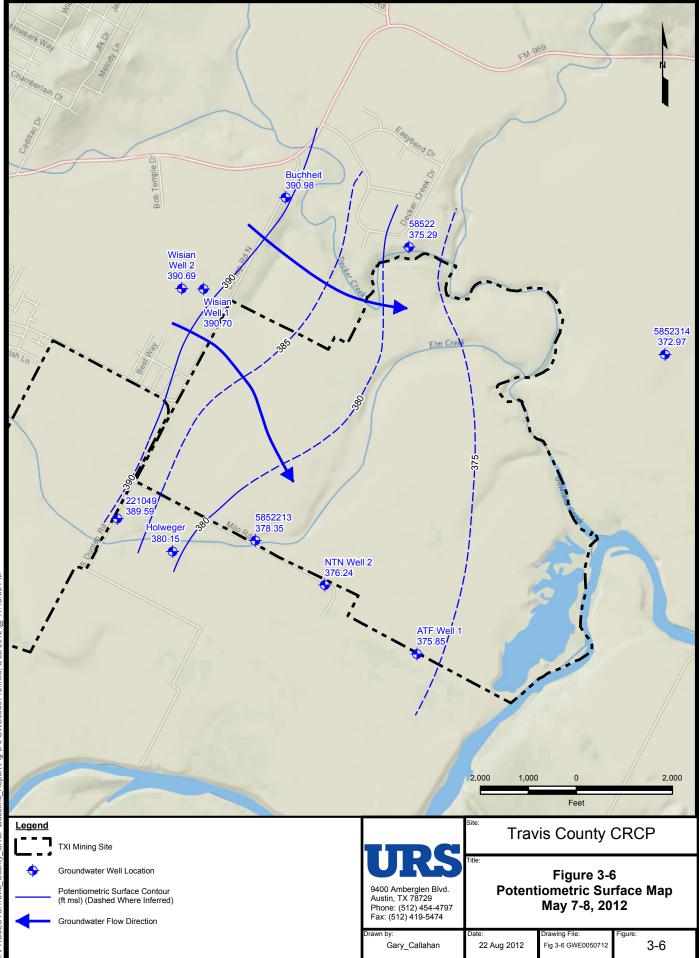




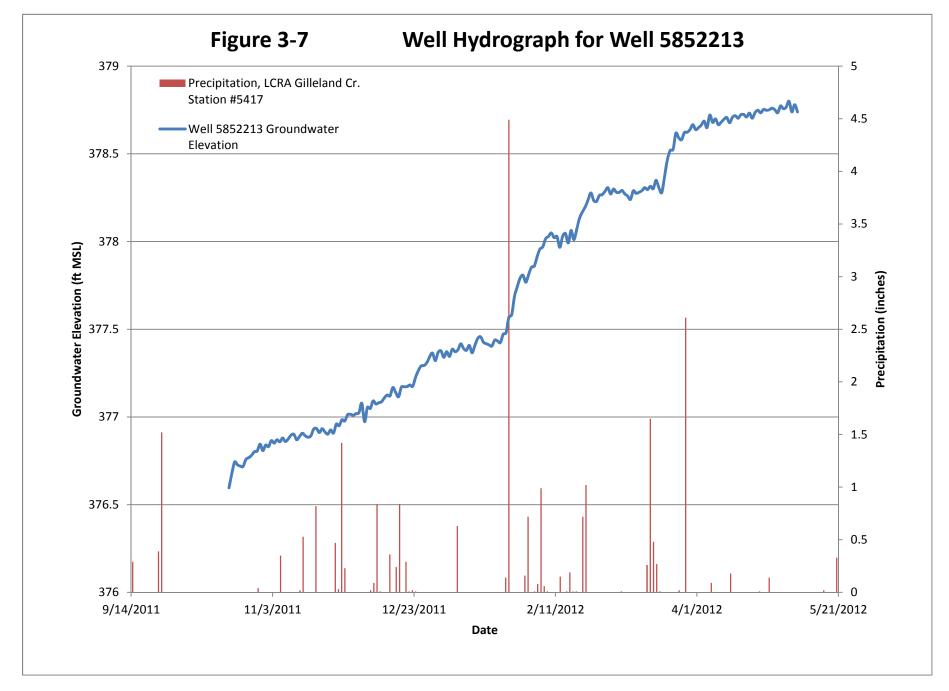


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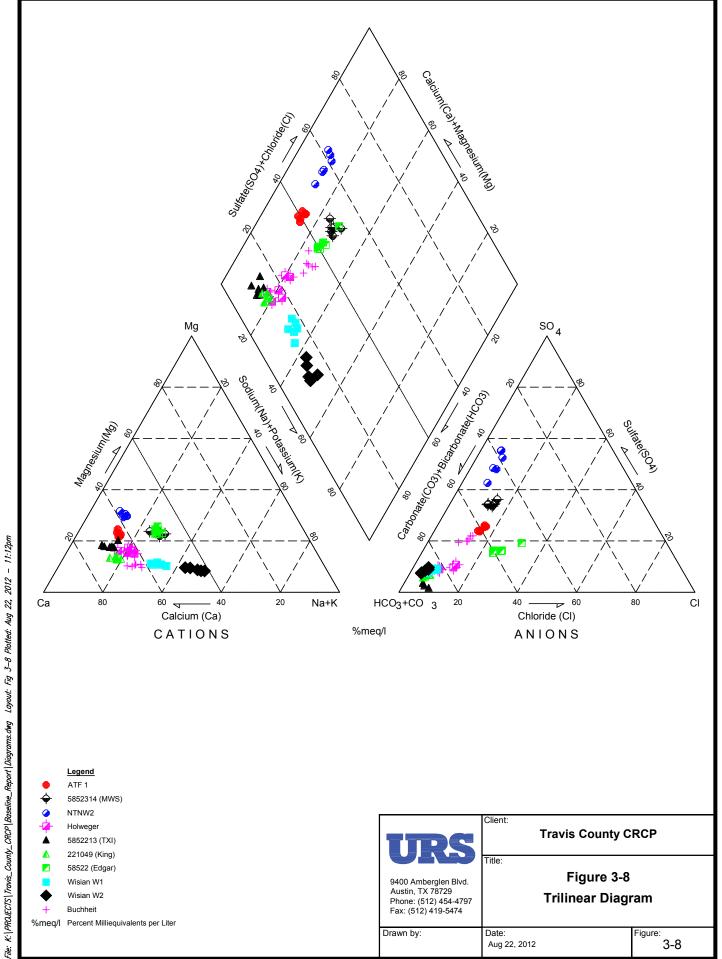
Baseline Report - Environmental Monitoring CRCP Travis County, Texas



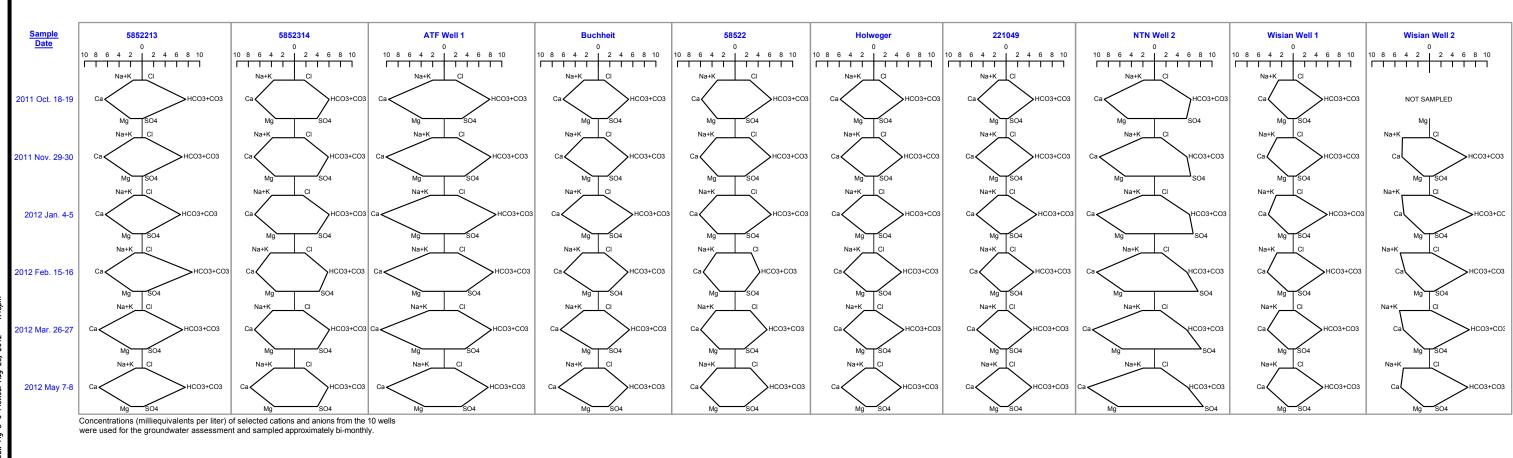
K:\PROJECTS\Travis_County_CRCP\Baseline_Report\Fig 3-6 GWE0050712.mxd, 8/22/2012 @ 11:45:33 PM



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URS	Client: Trav	vis County CRCP	
9400 Amberglen Blvd. Austin, TX 78729 Phone: (512) 454-4797 Fax: (512) 419-5474	Title:	Figure 3-9 Stiff Diagrams	
Drawn by: Gary_Callahan	Date: Aug 23, 2012	Drawing File: Diagrams.dwg	Figure: 3-9

August 2012

4.0 ENVIRONMENTAL MONITORING DATA EVALUTION

4.1 Task 1, Groundwater Evaluation

Baseline groundwater availability and quality conditions were evaluated using the groundwater data collected during the six approximately bi-monthly groundwater sampling events.

Groundwater Availability

The general groundwater flow direction of the Colorado River Alluvial Aquifer within the study area is towards the east and southeast with an average hydraulic gradient of 0.0023 (Figures 3-1 to 3-6). The groundwater flow direction appears to be influenced by pumping wells NTN Well 2, ATF Well 1 and well 5852314. Wells 5852314 and NTN Well 2 have the most significant influence on the potentiometric surface because of their daily cyclical pumping rates of approximately 670 gallons per minute (gpm) and 300 gpm respectively. Well ATF Well 1 has an approximate pumping rate of 450 gpm, but it not used on a regular basis. However, localized buried gravel channels within the Colorado Alluvial Aquifer may provide conduits for groundwater flow in directions not consistent with the general east-southeast groundwater flow direction. From October 2011 to May 2012 the groundwater elevation in the area rose in each of the 10 wells monitored. Table 4-1 shows the change in groundwater elevation at each well.

The rise in groundwater elevation is likely a recovery response caused by above average precipitation during November and December 2011, and January to March 2012 recharging the Colorado River Alluvial aquifer after the extreme dry conditions that persisted from February to October 2011. The 2011 rainfall total recorded at Austin Bergstrom International Airport (ABIA) was only 16.98 inches and well below the average yearly rainfall of 32.52 inches. Precipitation data from 1942 to 2012 at ABIA is included as Appendix D. Additionally, the observed groundwater elevation recorded with the transducer in well 5852213 shows marked increased water levels corresponding to precipitation events and relatively flat water level trends during periods of little or no precipitation (Figure 3-7).

Availability of groundwater for domestic, agricultural, and municipal use from the Colorado River Alluvial Aquifer is dependent upon the aquifer potentiometric surface remaining within or above the screened intervals of existing wells and is largely controlled by local precipitation recharge. Loss of groundwater elevation resulting in diminished or complete loss of groundwater availability was observed in the Glass well where only 0.22 to 0.40 ft of water was in the well (Table 3-1), and presumably was a result of dry climatic conditions. Not including the Glass well, the observed thickness of water in wells included in the monitoring program ranged from 4.23 ft (Buchheit Well on January 5, 2012) to 24.25 ft (Well ATF W 1 on March 27, 2012) (Table 3-1). Overall groundwater elevations ranged from approximately 390 ft above mean sea level (msl) upgradient of the Hornsby Bend East mine location to approximately 370 ft above msl downgradient (Figures 3-1 to 3-6).

Groundwater Quality

Water quality of the Colorado River Alluvial Aquifer in the vicinity of the Hornsby Bend East mine location was assessed by analyzing the groundwater for major-ions and nutrients. Major-ions were graphically evaluated to identify the typical water types present prior to mining, and a

statistical evaluation of major-ions and nutrient concentrations in groundwater was performed to identify the typical range of values present during baseline conditions.

Major-ion chemistry data was used to construct trilinear (Hem, 1992) and Stiff diagrams (Stiff, 1951). The trilinear diagram (Figure 3-8) depicts the water composition as percentage milliequivalents per liter (meq/L) and shows that the Colorado River Alluvial Aquifer groundwater is predominantly indicative of calcium-bicarbonate type water. However, three wells have a calcium-bicarbonate/calcium-sulfate mixed type water and one well has a calcium-bicarbonate/sodium-bicarbonate mixed type water. Wells 5852314, ATF 1 and NTN 2, which are located on the down gradient side of the study area have calcium-bicarbonate/calcium-sulfate mixed type water. Wisian Well 2 is the furthest upgradient well in the study area and shows calcium-bicarbonate/sodium-bicarbonate mixed type water.

Stiff diagrams (Figure 3-9) depict water composition as concentrations of meq/l for each of the 6 samples collected from the 10 wells. The similarity of the six stiff patterns from a single well indicates that no substantial temporal changes in major-ion chemistry occurred during baseline monitoring. This temporal consistency in major-ion chemistry at each well is also demonstrated by the tight pattern of plotted data for each well on the trilinear diagram (Figure 3-8).

A statistical evaluation of the water quality constituents for all wells is presented in Table 4-2 and the minimum, maximum and mean for each well in Table 4-3. Water quality data from the Glass well collected during the first sampling event on October 18, 2011 was not included in the statistical evaluation because the Glass well results are not indicative of the actual water quality of the Colorado River Alluvial Aquifer. Rather, it is suspected that the relatively elevated water quality concentrations of the constituents in Glass well (Table 3-2), calcium, potassium, and bicarbonate in particular, are indicative of stagnant water in the well sump.

The statistics of the water quality constituents were used to estimate a range of values representative of baseline conditions. As expected, the mean concentration for most constituents at the majority of the wells did not vary considerably from the overall mean (Table 4-3). Therefore, the range of concentrations (minimum to maximum) for each water quality constituent on Table 4-2 is representative of the overall baseline condition.

Water Quality Threshold Levels

An indication that a change from baseline water quality has occurred could be gained by comparing newly observed water quality values to the range of baseline values shown on Table 4-3. However, just because a hypothetical future water quality value may exceed its baseline maximum value does not necessarily indicate a change to baseline conditions. Natural variation in the baseline range obviously exits. Therefore, an approach to identify values that exceed baseline conditions would be to identify levels greater than the maximum baseline concentration plus one standard deviation. Values of maximum concentration plus one standard deviation are presented on Table 4-2.

4.2 Task 2, Air Quality Evaluation

Valid 24-hour PM_{10} and $PM_{2.5}$ mass measurement results are given in Table 3-3. The average levels of PM_{10} were 19.1 µg/m³ and 23.9 µg/m³ at the north and south sites, respectively. These

levels are slightly above the annual average PM_{10} level measured at 2600B Weberville Road, in East Austin, by TCEQ in 2011 (which was $18 \mu g/m^3$). The differences between the PM_{10} levels measured at the test sites relative to the East Austin annual average might be due to the different sampling schedules (TCEQ collects 24-hour PM_{10} and $PM_{2.5}$ filter samples once every six days throughout the year) or they may reflect an impact from windblown dust at the test sites due to the dry and mostly barren agricultural land nearby.

The average levels of $PM_{2.5}$ were 9.3 μ g/m³ and 10.5 μ g/m³ at the north and south sites, respectively. These levels are slightly below the 10.9 μ g/m³ annual average that TCEQ measured at Webberville Road in 2011. These small differences may also be attributed to the different sampling schedules or, perhaps, to less vehicular traffic near the test sites than near the East Austin monitor location.

Air Quality Threshold Levels

The 24-hour National Ambient Air Quality Standards (NAAQS) for $PM_{2.5}$ and PM_{10} are 35 $\mu g/m^3$ and 150 $\mu g/m^3$, respectively (40 CFR Part 50). All observed baseline $PM_{2.5}$ and PM_{10} levels were well below the levels of the respective NAAQS, though federal regulations call for three years of year round monitoring, at least once every six days, for determining compliance with the NAAQS. $PM_{2.5}$ and PM_{10} levels above these NAAQS may lead to adverse health effects, and reduced visibility. The NAAQS can be used in subsequent phases of this project for comparison to observed $PM_{2.5}$ and PM_{10} levels to asses potential air quality impacts associated with sand and gravel mining operations.

4.3 Task 3, Noise Assessment Data Evaluation

Noise is generally defined as unwanted sound that is typically associated with human activity and which interferes with or disrupts normal activities. Sound becomes unwanted when it interferes with our normal activities such as sleeping, conversation, recreation, or when it causes adverse health effects. Sound is created when objects vibrate, resulting in a rapid variation in surrounding atmospheric pressure called sound pressure. Airborne sound is generally described in terms of the amplitude and frequency of variation of air pressure. The standard unit of measurement of the amplitude of sound is the decibel (dB). Decibels are measured on a logarithmic scale representing points on a sharply rising curve. For example, 10 dB are 10 times more intense than 1 dB, 20 dB are 100 times more intense, and 30 dB are 1,000 times more intense.

Most of the sounds that humans hear in the environment do not consist of a single frequency, but rather a broad range of sound frequencies, with each frequency differing in sound level. The sound energy in each frequency add together to generate a sound. The method commonly used to quantify environmental sounds consists of evaluating all of the frequencies of a sound in accordance with a weighting that reflects the fact that human hearing is less sensitive at low frequencies and extreme high frequencies than in the mid-range frequency. This method is called "A-weighting", and the dB level so measured is called the A-weighted sound level (dBA). In practice, the level of a sound source is conveniently measured using a sound level meter that includes an electrical filter corresponding to the A-weighted curve. Typical A-weighted levels measured in the environment and in industry are shown in Table 4-4 for different types of noise.

All sound pressure levels decrease as a function of distance from the source as a result of wave divergence, ground attenuation, and atmospheric absorption. As a sound wave travels away from the source, the sound energy is dispersed over a greater area, thereby dispersing the sound energy of the wave over an increasing area. Intervening topography can have a substantial effect on sound pressure levels with greater ground attenuation occurring over rough terrain verses flat terrain. For example, noise levels for a line source such as a busy highway decrease 3 dBA over hard ground (concrete, pavement) or 4.5 dBA over soft ground (grass) for every doubling of distance between the source and the receptor. Atmospheric absorption also influences sound levels; the greater the distance traveled, the greater the influence and the resultant fluctuations. The degree of absorption is a function of the frequency of the sound as well as the humidity and temperature of the air. Atmospheric turbulence and meteorological conditions such as wind and temperature gradients can also play a significant role in determining the degree of attenuation.

Noise levels from construction activities or ground transportation sources depend on a number of factors including equipment type, volume and speed.

The existing noise environment near the future mining activity areas is affected by a number of noise sources, most of which are transportation-related (i.e., roadway and aircraft). Primary noise sources observed within the project area include FM 969, local residential roadways, and aircraft overflight operations from ABIA. Other sources of noise contributing to local noise background levels included agricultural activities including plant nursery, tree farming, and pecan orchards located on and south of Milo Road as well as general community noise from nearby residential areas.

The existing ambient baseline sound-level measurements for each monitoring location are shown in Table 4-5. The table lists the equivalent, or steady state average noise level equivalent steady-state sound level (L_{eq}) during the respective monitoring period for each round of noise monitoring.

As shown in Table 4-5, equivalent A-weighted sound levels vary greatly depending on location. Existing daytime noise levels at residential areas located away from FM 969 (M1 through M4 and M7) generally vary from approximately 40 dBA to as high as 55 dBA. Monitored areas located next to the more heavily traveled FM 969 roadway (M5 and M6) are considerably higher varying from approximately 57 dBA to approximately 68 dBA.

A long-term (i.e., 4-hour) baseline noise measurement was also performed at the M1 measurement location. The noise measurement was conducted on a weekday, during the late afternoon hours. The resulting ambient noise level was 46.8 dBA which is very close (i.e., within 2 dBA) of the average of the short-term noise levels recorded at this same location.

Noise Threshold Levels

The project area is located within the Extra Territorial Jurisdiction (ETJ) of the City of Austin, therefore, the City of Austin noise ordinance applies. The City of Austin codifies noise regulations in several locations within its Code of Ordinances. Most references to noise concern music venues or the operation of sound equipment (loud speakers or public address systems) which do not apply to this project. However, some sections of the code may potentially apply to

TXI operations. In Chapter 9-2-3 – Noise and Amplified Sound, General Restrictions, Section 9-2-3(2) prohibits the "making of noise audible to an adjacent business or residence between 10:30 PM and 7:00 AM". Section 9-2-3(3) prohibits "operation of a machine that separates, gathers, grades, loads, or unloads sand, rock, or gravel within 600 feet of a residence, church, hospital, hotel, or motel between 7:00 p.m. and 6:00 a.m.".

Other sections within the Code of Ordinances prohibit certain noise levels and conditions within Planned Development Areas and Traditional Neighborhood Districts; however, at this time the surrounding residential areas do not qualify for these designations.

No standardized or regulatory criteria have been developed for specifically assessing construction noise impacts. Therefore, criteria must be developed on a project-specific basis unless local ordinances can be found to apply. Outside of work hour and distance requirements as shown above, the City of Austin noise ordinances do not specifically apply to construction noise levels within the project area and are therefore, not practical for assessing the noise impact of a construction project.

Project construction noise threshold levels should take into account existing noise levels, adjacent land use, and the duration of construction activities. The Federal Transit Administration (FTA) has developed general project construction noise criteria guidelines that can be considered reasonable criteria to be used in construction noise assessments. For general construction noise assessments, the eight-hour L_{eq} dBA noise criteria levels for various land use activity categories provided in Table 4-6 are often used.

Noise levels above these threshold criteria may lead to adverse community reaction, while noise levels below them generally require no action. The FTA noise criteria or other applicable construction noise criteria should be used in subsequent phases of this project to predict potential noise impacts associated with sand and gravel mining operations.

Table 4-1. Observed Groundwater ElevationIncrease from October 2011 to May 2012

Well ID	Change in Groundwater Elevation (ft)
58522	+ 0.17
221049	+ 1.42
5852213	+ 1.88
5852314	+ 4.85
ATF Well 1	+ 1.75
Buchheit	+ 1.83
Holweger	+ 1.44
NTN Well 2	+ 3.49
Wisian Well 1	+ 0.85
Wisian Well 2	+ 0.67

ATF - Austin Tree Farm. ft - feet, foot. ID - Identification. NTN - Native Texas Nursery.

Overall Statistic (all normal samples)	Calcium (mg/L)	Magnesium (mg/L)	Potassium (mg/L)	Sodium (mg/L)	Chloride (mg/L)	Fluoride (mg/L)	Nitrate (mg/L)	Sulfate (mg/L)	Bicarbonate (mg/L)	Carbonate (mg/L)	Ammonia (mg/L)	TSS (mg/L)	TDS (mg/L)
# of Samples	59	59	59	59	59	59	59	59	59	59	59	59	59
Mean	134	27.3	2.71	57.0	38.9	0.28	10.5	99.3	364	< 2	0.28	5.13	724
Range	149	66.6	4.21	95.4	89.4	0.32	34.7	399	285	< 2	6.33	72.7	709
Minimum	84	10.1	1.80	22.6	10.2	0.11	0.01	7.11	259	< 2	0.02	1.00	440
Maximum	233	76.7	6.01	118	99.6	0.43	34.7	406	544	< 2	6.35	73.7	1149
Standard Deviation	41	17.9	0.94	24.2	27.7	0.09	8.19	103	69.9	< 2	0.99	12.6	205
Mean + 1 Standard Deviation	175	45.2	3.63	81.2	66.6	0.37	18.7	202	433	< 2	1.27	17.7	929
Mean + 2 Standard Deviations	216	63.1	4.58	105	94.2	0.45	26.9	305	503	< 2	2.26	30.3	1134
Maximum + 1 Standard Deviation	274	94.6	6.95	142	127	0.52	42.9	509	614	< 2	7.34	86.3	1354

Table 4-2. Overall Water Quality Statistics

mg/L - Milligrams per liter.

TDS - Total dissolved solids.

TSS - Total suspended solids.

Well ID	Minimum/Maxim um	Calcium (mg/L)	Magnesium (mg/L)	Potassium (mg/L)	Sodium (mg/L)	Chloride (mg/L)	Fluoride (mg/L)	Nitrate (mg/L)	Sulfate (mg/L)	Bicarbonate (mg/L)	Carbonate (mg/L)	Ammonia (mg/L)	TSS (mg/L)	TDS (mg/L)
	Minimum	194	41.2	3.48	43.2	65.2	0.14	4.86	143	461	< 2	0.02	1.00	967
ATF 1	Mean	208	45.4	3.93	50.7	77.3	0.23	6.76	165	497	< 2	0.03	1.37	1050
	Maximum	222	47.3	4.49	57.4	83.6	0.36	8.91	184	544	< 2	0.07	2.30	1123
	Minimum	134	36.8	1.98	79.4	52.2	0.17	10.3	187	349	< 2	0.02	1.10	871
5852314	Mean	140	39.9	2.20	85.9	58.8	0.24	10.9	193	359	< 2	0.02	1.58	881
	Maximum	154	42.5	2.53	94.5	63.8	0.30	11.2	207	368	< 2	0.02	2.30	891
	Minimum	175	56.5	2.24	41.7	35.6	0.20	24.3	266	336	< 2	0.02	1.00	965
NTNW2	Mean	208	64.8	2.36	46.7	39.4	0.29	29.1	342	352	< 2	0.02	1.03	1052
	Maximum	233	76.7	2.51	52.6	44.9	0.42	34.7	406	382	< 2	0.03	1.10	1149
	Minimum	105	15.3	1.88	31.9	11.8	0.29	15.2	21.1	287	< 2	0.02	1.00	484
Holweger	Mean	111	17.0	1.97	40.0	21.1	0.33	18.0	27.3	302	< 2	0.02	1.07	522
	Maximum	117	19.7	2.03	45.2	32.6	0.43	21.6	34.1	314	< 2	0.02	1.10	556
	Minimum	128	20.1	4.35	22.6	15.2	0.23	0.01	7.11	404	< 2	0.91	5.90	633
5852213	Mean	137	22.2	4.80	27.4	18.9	0.31	0.05	21.9	449	< 2	2.58	31.7	682
	Maximum	150	24.8	6.01	31.9	27.8	0.39	0.10	37.4	527	< 2	6.35	73.7	759
	Minimum	92.7	10.9	1.80	25.8	10.2	0.18	12.9	14.9	267	< 2	0.02	2.90	440
221049	Mean	102	12.0	1.88	29.2	12.1	0.28	13.5	16.8	286	< 2	0.02	7.95	462
	Maximum	106	13.1	2.01	30.5	14.2	0.43	14.2	18.5	320	< 2	0.02	17.9	498
	Minimum	111	32.1	1.84	69.5	87.8	0.20	2.42	76.1	259	< 2	0.02	1.00	661
58522	Mean	119	34.8	2.04	72.4	91.8	0.26	3.40	78.9	346	< 2	0.02	2.03	747
	Maximum	124	37.5	2.23	75.2	99.6	0.32	4.27	81.3	382	< 2	0.02	3.80	784
Wisian	Minimum	86.6	10.1	2.61	53.9	12.7	0.24	8.03	21.2	300	< 2	0.02	1.00	493
Wisian W1	Mean	89.5	10.6	2.77	59.5	16.0	0.29	8.66	25.4	318	< 2	0.02	1.53	523
VV 1	Maximum	92.2	11.0	3.04	66.1	19.2	0.41	8.88	27.5	356	< 2	0.02	2.40	562
Wisian	Minimum	83.9	10.2	2.41	66.1	10.6	0.11	8.88	27.5	356	< 2	0.02	1.00	651
Wisian W2	Mean	91.6	11.2	2.51	110	12.8	0.13	11.0	31.72	413	< 2	0.02	1.30	675
vv∠	Maximum	99.4	12.2	2.72	118	15.3	0.14	12.5	36.2	455	< 2	0.02	1.80	710
	Minimum	117	11.4	2.30	53.6	31.8	0.28	3.73	76.0	310	< 2	0.02	1.00	618
Burchheit	Mean	126	12.5	2.44	57.0	36.7	0.36	4.19	80.2	324	< 2	0.02	1.05	641
	Maximum	139	13.0	2.59	61.5	39.9	0.39	4.70	85.2	363	< 2	0.05	1.20	678
All Wells	Overall Mean	134	27.3	2.71	57.0	38.9	0.28	10.5	99.4	364	< 2	0.28^{1}	5.13	724

Table 4-3. Water Quality Statistics by Well

Note:

¹Overall ammonia mean skewed by well 5852314, overall ammonia mean without 5852314 is 0.02.

ATF - Austin Tree Farm.

ID - Identification.

mg/L - Milligrams per liter. NTN - Native Texas Nursery. TDS - Total dissolved solids.

TSS - Total suspended solids.

Table 4-4. Range of Common Sound Levels on an A-Weighted Decibel Scale

Outdoor	dBA	Indoor
Jet takeoff at 200 feet/car	120	Threshold of pain
Horn at 3 feet		
Pneumatic hammer	100	Subway train
Gas lawn mower at 3 feet		
	90	Food blender at 3 feet
Downtown (large city)	80	Garbage disposal at 3 feet
Lawn mower at 100 feet	70	Vacuum cleaner at 10 feet
		Normal speech at 3 feet
Air conditioning unit	60	Clothes dryer at 3 feet
Babbling brook		Large business office
Quiet urban (daytime)	50	Dishwasher (next room)
Quiet urban (nighttime)	30	Recording studio
	0	Threshold of hearing

Source: FHWA, 1997.

Table 4-5. Summary of Daytime Ambient Noise Measurements

		Monitored Noise Level (dBA Leq)											
			Rou	und 1	Round 2								
Site													
Location	10/26	10/27	10/28	10/31	11/2	11/3	3/22	3/23	3/28	3/29	3/30		
M1	47.0	53.6	51.0	50.4	53.1	55.5	45.5	42.7	52.6	44.4	44.0		
M2	43.8	48.2	51.0	41.2	44.8	53.5	49.4	49.7	44.2	45.8	44.5		
M3	42.1	46.9	46.6	43.7	47.5	47.6	51.3	44.4	44.3	47.1	41.6		
M4	48.3	48.6	50.5	43.6	48.8	49.3	50.4	44.3	48.2	43.3	42.5		
M5	59.6	59.9	59.1	58.2	61.6	60.8	57.6	58.9	58.5	56.7	56.8		
M6	66.1	62.7	65.2	65.8	65.8	62.3	67.1	64.1	67.2	68.3	63.8		
M7	39.7	47.2	52.4	46.0	48.7	43.3	44.7	41.6	53.5	45.7	45.2		

Table 4-6. Federal Transit Administration Construction Noise Criteria Guidelines

	Eight-hour Leq (dBA)					
Land Use	Day	Night				
Residential	80	70				
Commercial	85	85				
Industrial	90	90				

Source: FHWA, 2006.

5.0 CONCLUSIONS AND RECOMMENDATIONS

The following section presents the conclusions and recommendations of the baseline environmental monitoring for groundwater, air, and noise.

5.1 Conclusions

Groundwater

Baseline groundwater availability conditions of the Colorado River Alluvial Aquifer in the vicinity of the Hornsby Bend East and Hornsby Bend West mine location indicate that groundwater flow is to the south and southeast, with a typical potentiometric surface of approximately 390 ft above msl on the west to approximately 370 ft above msl on the east. Groundwater elevations in the area were rising as winter and spring 2012 precipitation recharged the aquifer after an abnormally dry summer and fall of 2011.

Typical groundwater at the site is calcium-bicarbonate type water. One upgradient well (Wisian Well 2) exhibited calcium-bicarbonate/sodium-bicarbonate mixed type water and three downgradient wells (5852314, ATF 1, and NTN 2) exhibited calcium-bicarbonate/calcium-sulfate mixed type water. Despite the presence of the mixed water types located on the up and downgradient ends of the site, the overall range of water quality constitutes is relatively consistent and appears representative of baseline water quality conditions. The minimum to maximum ranges of water quality constituents on Table 4-2 are indicative of baseline water quality conditions. The maximum water quality values plus one standard deviation can be used as a criteria to determine if baseline levels have been exceeded.

Air

 $PM_{2.5}$ and PM_{10} levels from both locations averaged 9.8 µg/m³ and 21.1 µg/m³, respectively. These levels are consistent with the annual average $PM_{2.5}$ and PM_{10} level measured at 2600B Weberville Road, in East Austin, by TCEQ in 2011, which were 10.9 µg/m³ and 18.0 µg/m³, respectively. The small differences between the air quality levels measured at the test sites relative to the East Austin annual averages might be due to different sampling schedules or local effects such as windblown dust from dry agricultural land at the site (PM_{10}) and perhaps less $PM_{2.5}$ impact due to less vehicular traffic near the test site relative to the East Austin monitor location. All observed baseline $PM_{2.5}$ and PM_{10} levels were well below the NAAQS of $35\mu g/m^3$ for $PM_{2.5}$ and $150 \mu g/m^3$ for PM_{10} .

The $PM_{2.5}$ and PM_{10} air quality levels shown in Table 3-3 will serve as a comparison tool for future air quality levels during subsequent phases of the project to determine potential air impacts once mining operations begin.

Noise

Existing noise levels within the project area vary greatly depending on location with the highest noise levels occurring adjacent to FM 969 and Dunlap Road and lower noise levels occurring in the more rural sections of the project study area. Measured daytime noise levels within the study area are consistent with normal daytime noise levels for quiet urban and suburban areas of approximately 50 dBA as shown in Table 4-5.

The noise levels shown in Table 4-6 will serve as a comparison tool to future noise levels during subsequent phases of the project to determine potential noise impacts in adjacent residential areas once mining operations begin. Potential noise impacts should be determined based on future TXI mining activities, including proposed operations, schedules, and equipment to be used.

5.2 Recommendations

Groundwater

Prior to initiation of active mining operations at the Hornsby Bend East and Hornsby Bend West sites, it is recommended that groundwater levels be measured quarterly at the same 10 wells included in the baseline monitoring and that continuous water level monitoring at well 5852213 be continued. Groundwater sampling from the 10 wells should be performed annually until active mining commences. The water quality and groundwater availability data collected during this interim mining period should be used to update and or adjust baseline values. Once active mining starts it is recommended that water quality and groundwater availability monitoring be conducted quarterly.

Air

It is recommended that air quality sampling for $PM_{2.5}$ and PM_{10} from the same two locations used for the baseline sampling be performed quarterly for the first two years of active mining.

Noise

Prior to the start of future TXI mining activities, potential noise impacts associated with future mining activities should be determined at nearby off-property sensitive receptor locations. For best results, TXI operational parameters for the Hornsby Bend East and Hornsby Bend West sites should be well established. If noise impacts are predicted, then noise abatement measures should be considered. A noise abatement measure is any positive action taken to reduce the impact of noise on an activity area such as source controls (e.g., varying haul road paths), pathway controls (e.g., noise barrier walls, earthen berms, etc.), or receiver controls (e.g., acoustical land-use site planning concepts or acoustical construction techniques). Once active mining starts, it is recommended that noise monitoring be conducted semi-annually for the first year of mining.

6.0 REFERENCES

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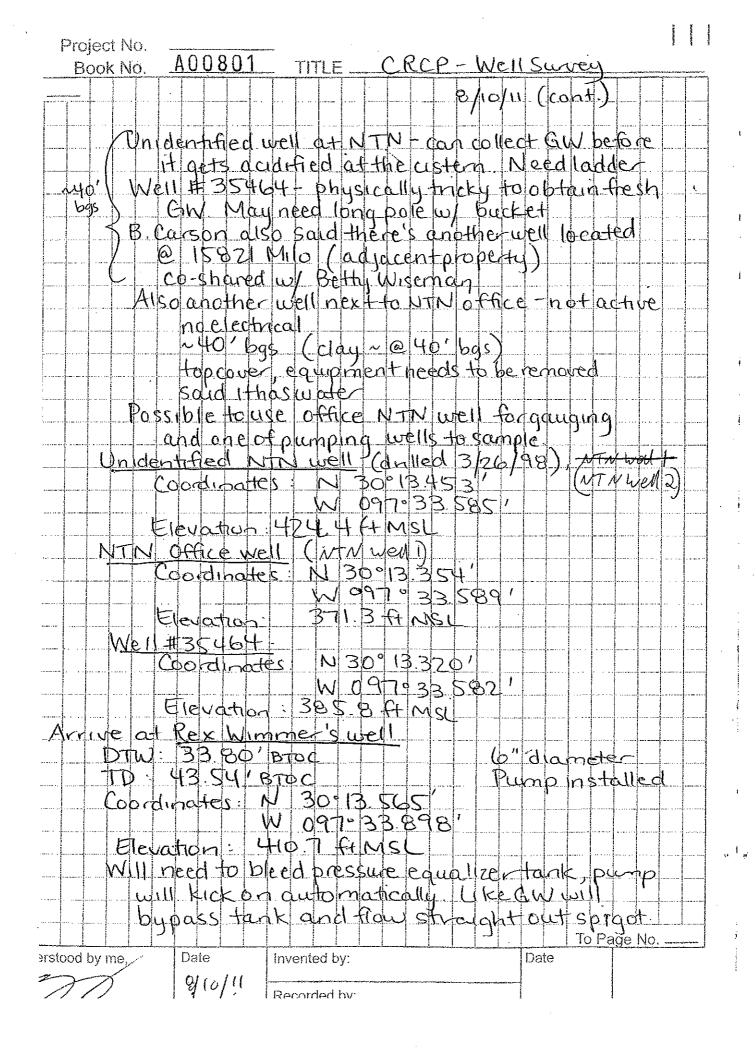
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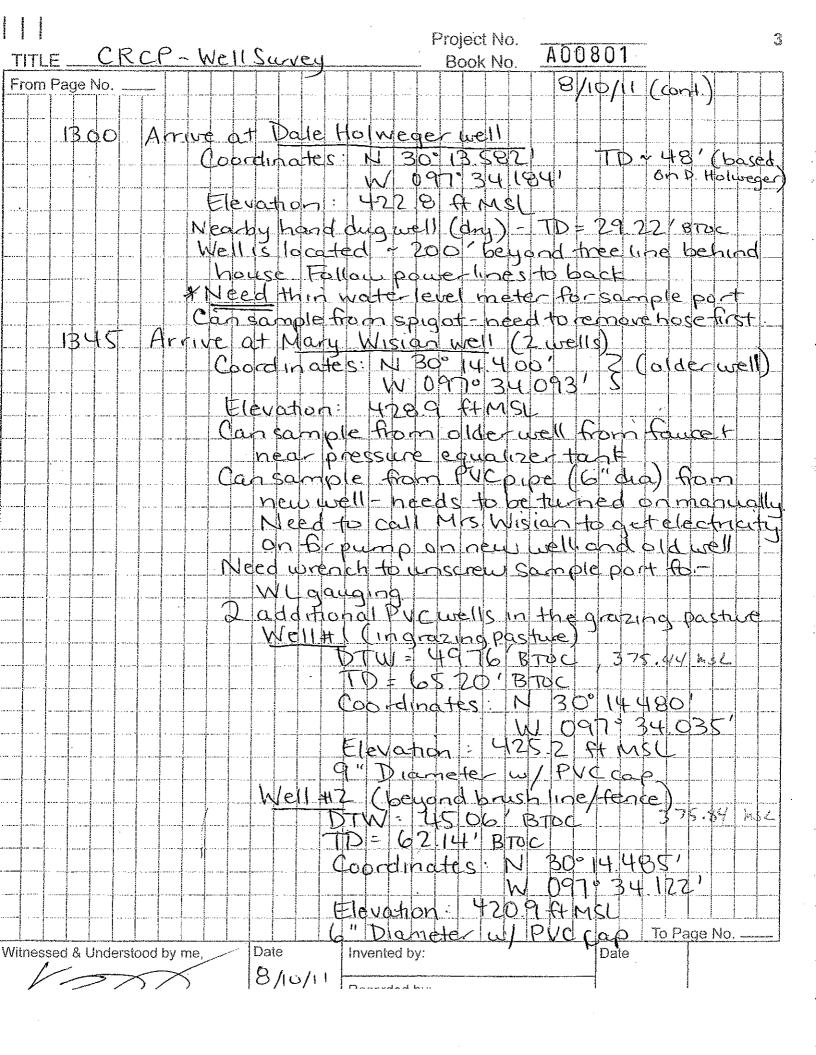
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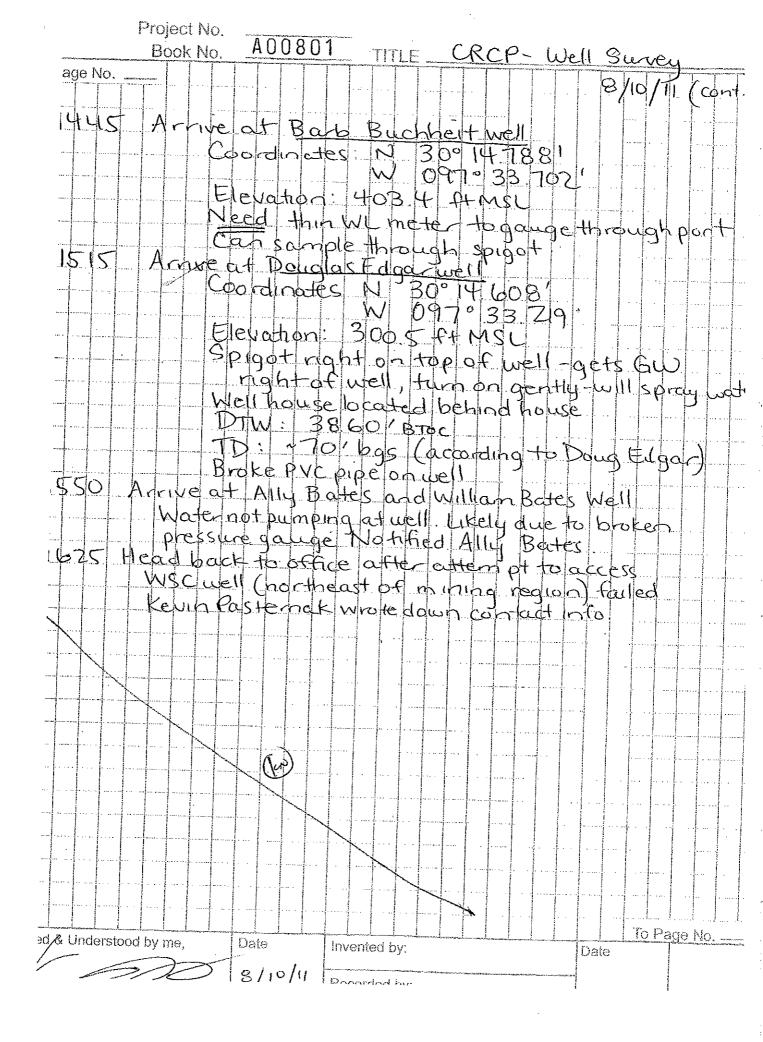
APPENDIX A

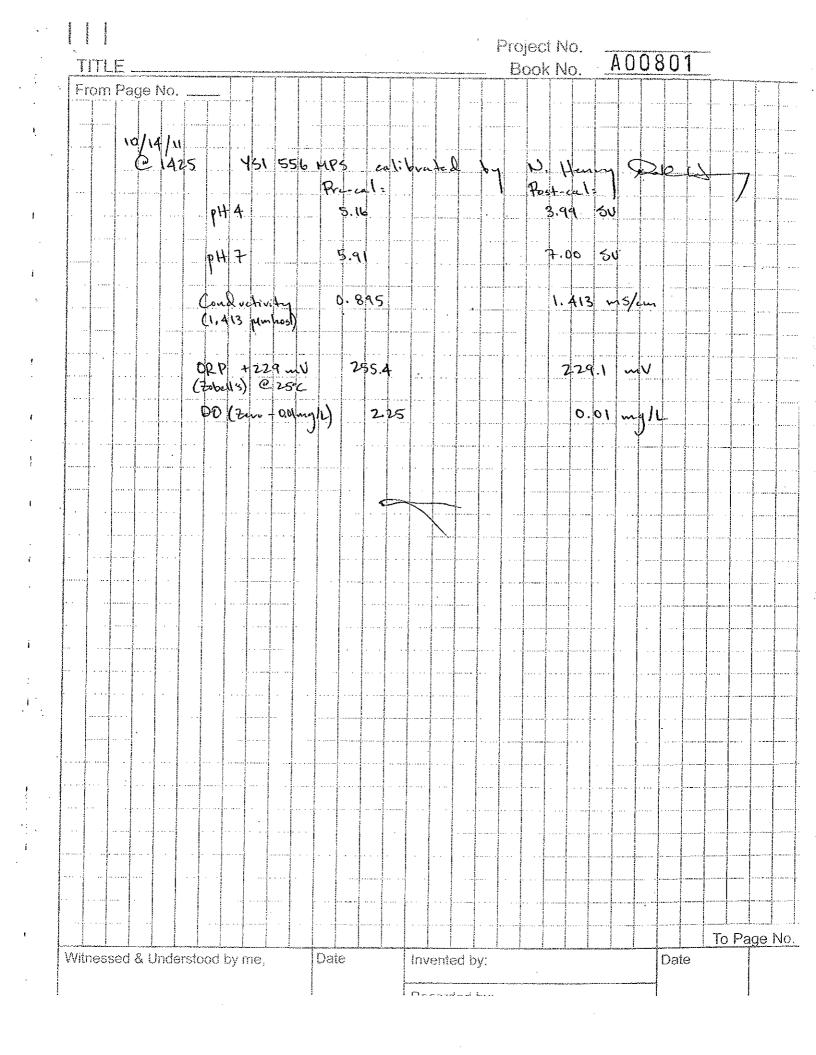
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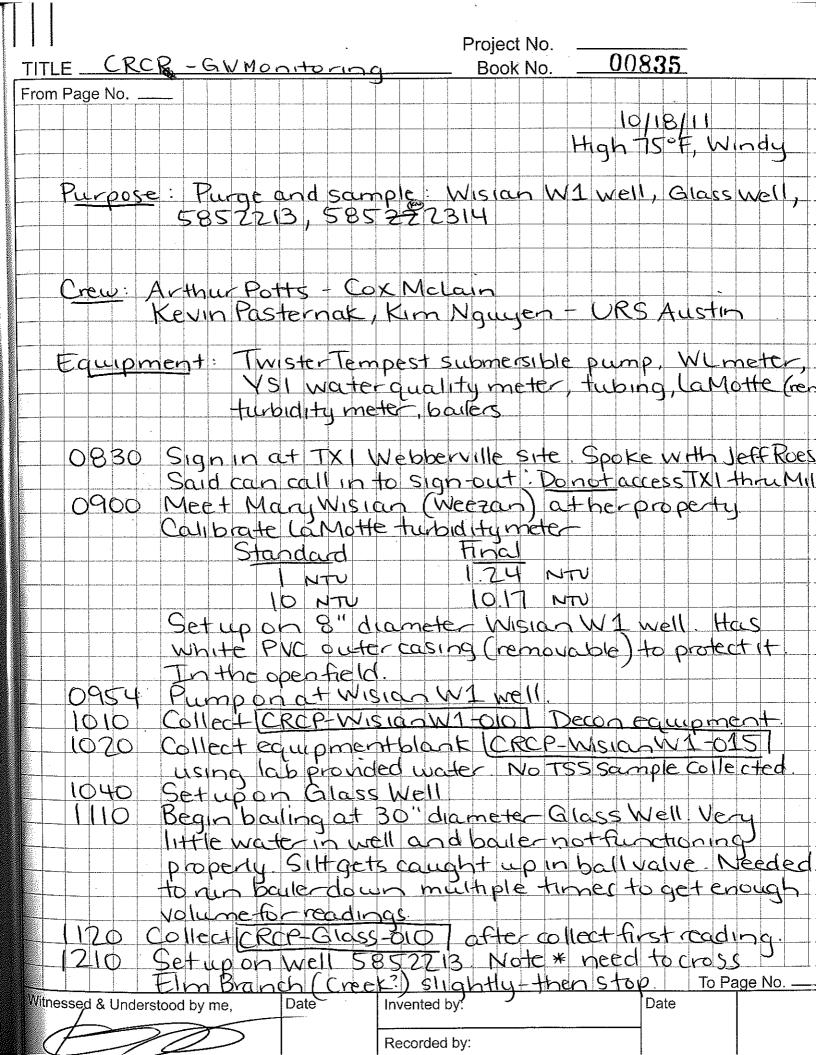
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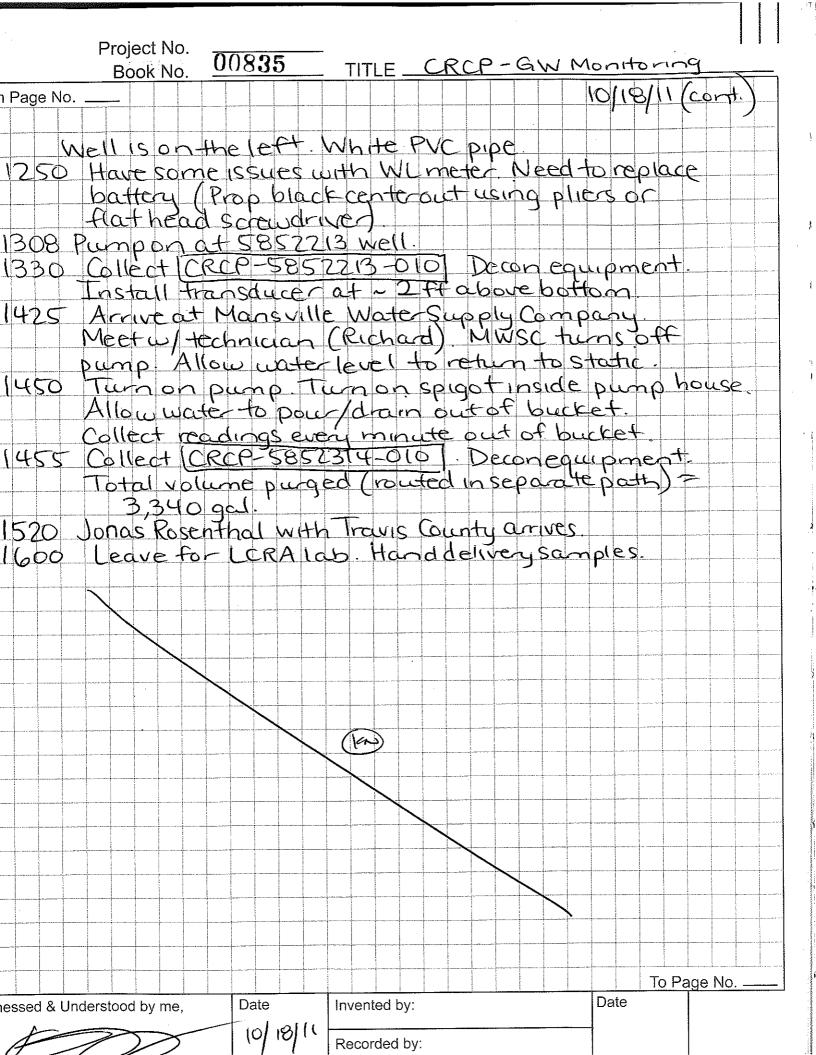










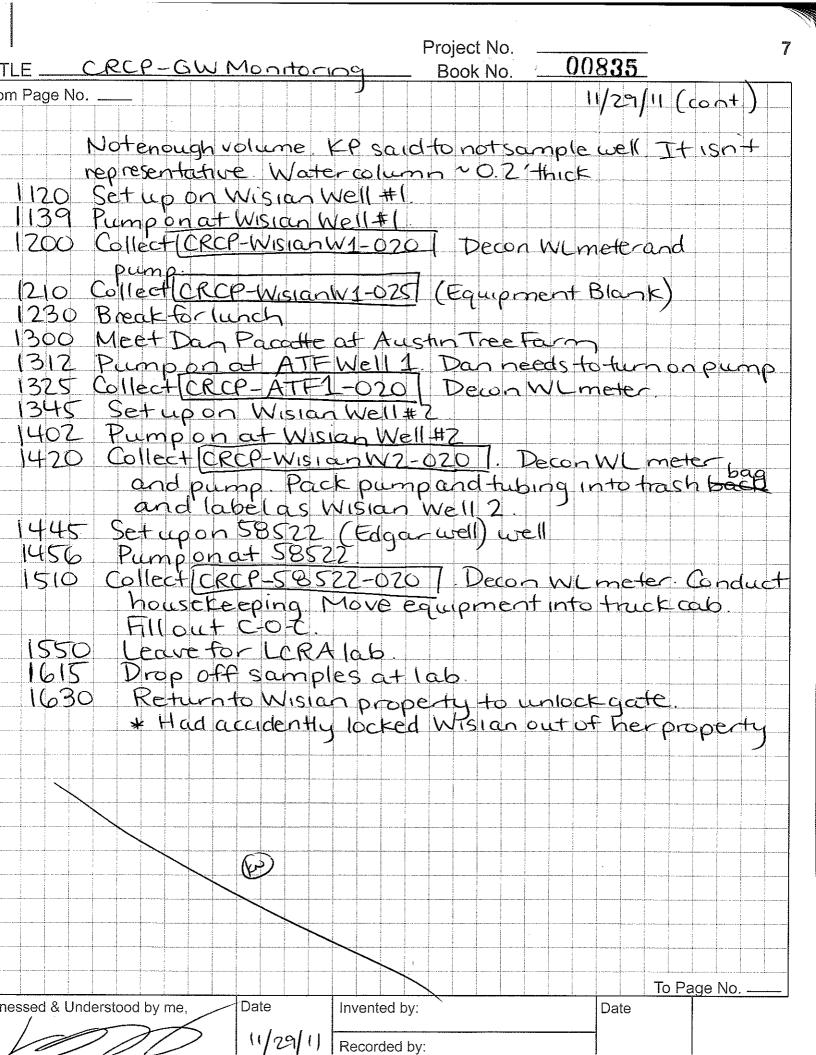


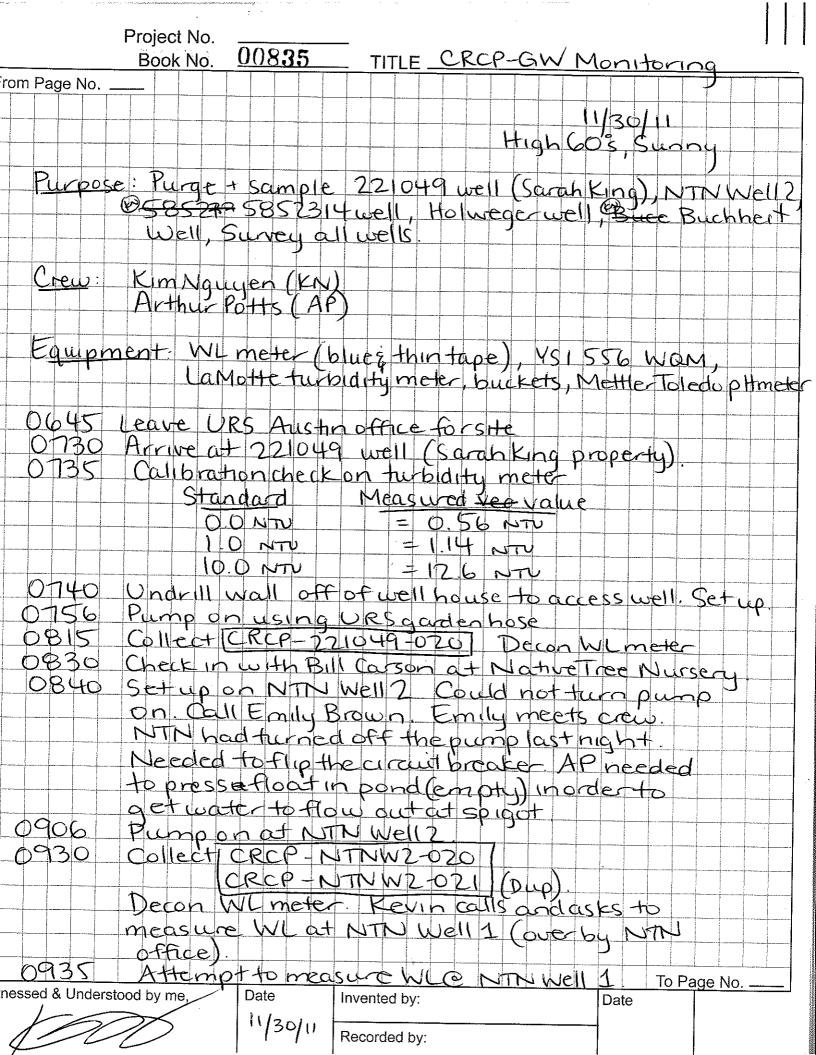
Project No. 00835 CRCP-GW Monitoring TITLE . Book No. 10/19/11 From Page No. High 75°F, Sunny Purpose: Purge and sample 221049 well (Sarah King), Buchertwell, 58522 (Edgar), NTN Well 2, ATF Well !! Holwegerwell Equipment: YSI water quality meter (URS property) blue WL meter (URSproperty), thin tape WL meter (URS property), La Motte turbidity meter (Ashtead rental), buckets, dedicated private pumps Arthur Potts (Cox Mclain) Crew KimNguyen, Kevin Pasternat (URS Austin) 0715 AP & KN leave from URS office for site Purchase ice. 0755 Arrive at Sarah King's house - 221049 well. Talk to Sarah King about her pressurized tank. Said Hoesnitwork. Pump Kicks on everytime she turns on water. Mater doesn't fill up tank. Since tank doesn't work. Good because URS doesn't need to drain tank before sampling. Use spigot on back of well house. > Spigot attached to a garden hose Turn spigot on. Collect readings Collect CRCP-221049-0101 * WL was stable 0826 0840 *Note * Do not run over cat when driving in /out of drive way. 0810 Calibrate La Motte turbidity meter KP said YSI doesn't need to be calibrated 0900 Arthur and Randy Stephens (URS) goes to Wislan property to set up air monitoring equipment. KP helps setup 0930 Set up on Bucheit well. Purge water from spigot Turn spigoton. No hose Collect CRCP-Bucheit-010 6941 1000 To Page No. -Witnessed & Understood by me, Date Invented by: Date 10/18/11 Recorded by:

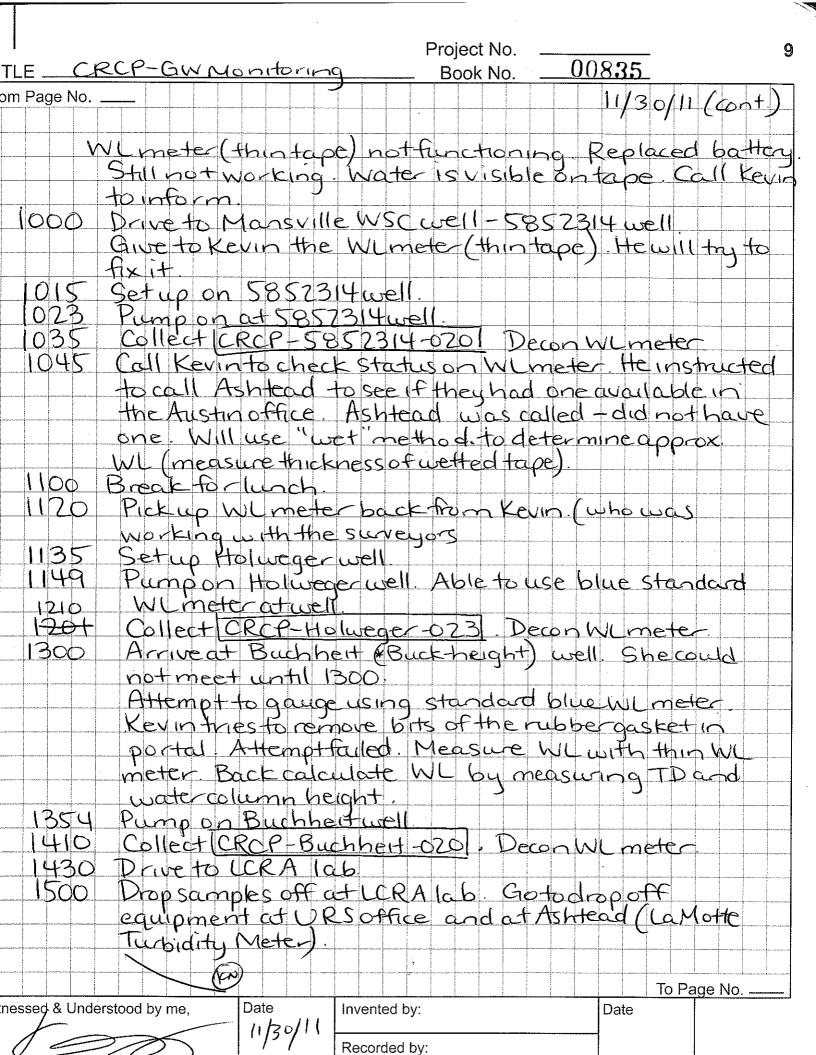
Project No. 00835 TITLE CRCP-GW Monitoring Book No. rom Page No. 10/19/11 (cont.) 1015 Jonas with Travis County meets URS at Exxon Set up on 58522 well (Douglas Edgar) Discuss with DE about drilling hole into cap to run WU 1030 meter down. Will need to plug hole with 3/4" plug 1138 Spigoton at 58522 well. DE needs to turn power to pump on from the house Run water through hose (belonging to DE) 1150 Collect CRCP-58522-0101 1200 Meet AP and RS at Native Tree Nursery (NTN) Check in with Emily Brown 1230 Measure DTW at NFN Well 1 (well by office) DTW = 30.63 Broc TD = 36.16'BTOC 123500 Set up on NTN Well Z. Water discharges from outfall. Pumprate will vary based on level in pond. Move/ Submerge float" If need pump to start. Flow rate averagetby reading total volume (on meterinside pump housing) and dividing over time Begin taking readings at NTN Well 2. Collect (CRCP-NTNW2-010) 1249 1255 Arrive at Austin Tree Farm (ATF) KP discusses 1310 with AP and RS about potential airmonitoring locations. Meet u/ manager of ATF-Dan Turn on pump. Need some time to allow water-1340 to reach & Hose was on spigot Turn on spigot 1355 Collect (CRCP-ATF1-010 Set upon Holwegerwell. Can use large WL meter 1410 If unscrew pink-top. Sample from spigot by unscrewing piping. Turn spigoton 1448 Collect' CRCP-Holweger-010 1455 Conduct housekeeping Complete COC 1515 600 Delwery samples to URA lab (ELS) To Page No. itnessed & Understood by me Date Invented by: Date 10/19/11 Recorded by:

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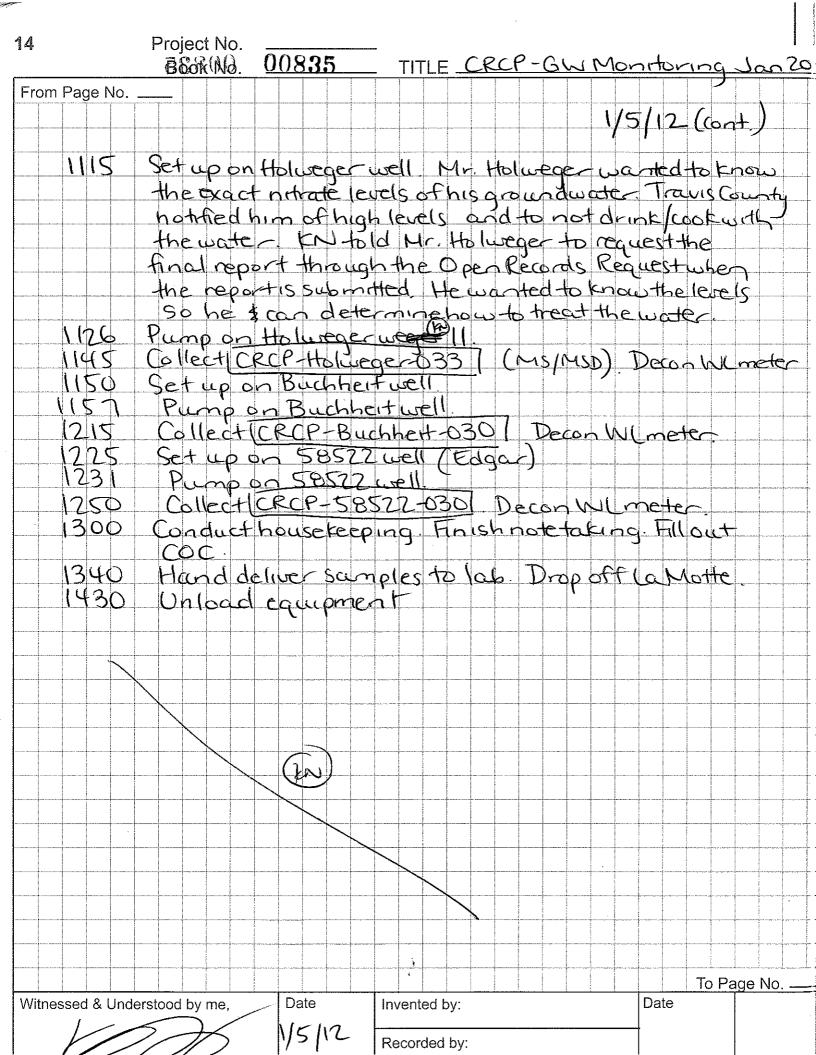


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13 Project No. 00835 LE CRCP-GW Monitoring Jan 2012 Book No. n Page No. 1/5/12 Clearskies, High 60's Purpose Purge + sample well 2210 49 (sarah King), Holweger well, ATF Well I, NTN Well 2, Buchheitwell Weil 58522 (Edgarwell) Equipment: YSI 556 WQ meter, Mettler ToledopH meter, La Motte hubidity mater blue WL meter thin tape WI meter Kim Nguyen (KN) - URS Austin Crew Arthur Potts (AP) - Cox Malain Meet at URS Drive to well 221049 (Sarahking) well 0645 0750 Set up on well 221049 0811 Pumpon at well 221049 . Deconthin tape WL 0830 Collect CRCP-221049-030] meter 0900 Purchase ice for cooler. Fuel up truck. Set upon ATFWell I. Call Dan Pacatte to inform He said to alsk one of workers to turn on the pump 0915 because he will not be able to come 0929 Pumpon at ATF Well 1 Collect |CRCP-ATF1-030] Deconblue WL meter 0950 Measure DTW at NTN Well 1 (by office) 1000 DTW = 29.36 BTOC TD = 36.19 BTOC Decan thin tape WL meter [015]Set up on NTN Well 2. Emily Brownsaid that pump was turned off the day before to allow for WL'to reach static levels. Just need to switch braker (labeled for pump) to one (three connected switches located on the left wall in pump house) 1021 Pumpon at NTN Well 200 1040 Collect CRCP-NTNWer2-030 [CRCP-NTNWZ-031] (DUP) Decon blue WL meter .! Break forlunch 1100 To Page No. essed & Understood by me, Date Invented by: Date 1/5/12 Recorded by:



41010113.102 Project No. 00835_____TITLE CRCP-GW Monitoring Feb 2012 16 Book No. 2/15/12 From Page No. _ High 72°F, Fog, Rain Purpose Purge + Sample ATF Well 1 5852213 (TXI Well), WisianWell 1, Wisian Well 2, 58522 (Edgar), 221049 (King) Equipment: Portable battery, Submersible pump, dedicated tubing blue WL meter thin tape WL meter, VSISS6 WQM, Mettler ToledopH meter, lowflow controller, l'amotte turbidity meter buckets Crew: KimNguyen (KN) · URS Austin ArthurPotts (AP) - CoxMelain 0700 Meet at URS office. Load equipment and supplies Go to LCRA lab to pick up coolers. 0840 Signinat TXI weberville plant. 0845 Meet Dan Pacette at ATFWell I. Kevin Pasternak Isonsite with Tom (TravisCounty) and Dr. Jack Sharp. Set upon ATF Well 1. Calibrate La Motte turbidity meter Standard Final Reading = 1.0 NTU = 0.97 NTU = 9 98 NTV = 10.0 NTU Pumpon at ATF Well 1 0906 Collect (CRCP-ATF1-040) Decon Wlmeter Set upon 5852213 (TXI well). Download 0920 0935 transducer data Pumponat 5852213 Conduct low flow purge 1007 Collect [CRCP-5852213-010] Decon WI meter + pum 020 Set up on Wisian Well 1. 1050 Pump on at Wisian Well- Conduct low flow purge Collect <u>CRCP-WisianW1-0401</u>. Decon W1 meter + per Collect equipment blank <u>CRCP-WisianW1-0457</u> Kevin, Tom, Jack head over to Glass Well to check On water level. DTW = 40.00 'BToc. KN and AP 105 1120 135 145 Set up on Wisian Well2 1159Pump on Wisian Well 2Conduct low flow purge.1215Collect CRCP-Wisian W2-0401Rinse pump To Page No.Witnessed & Understood by me,DateInvented by: 2/15/12 Recorded by: 12

