

January 29, 2018

Ms. Corazon Urgena, P.E. Austin Fire Department Emergency Prevention Division 505 Barton Springs Road, Suite 200 Austin, TX 78704 Via E-mail to: cora.urgena@austintexas.gov

RE: Development Near A Hazardous Pipeline Ordinance Compliance – Revision 1

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Ms. Urgena,

The purpose of this letter is to summarize how the subject property complies with the City of Austin Code of Ordinances §25-2-516 Development Near A Hazardous Pipeline (DNHP), Part (B) (1) Sections (a) through (j). For the purposes of this letter, use of the term "hazardous pipeline", or "pipeline" refers to that as defined in, and regulated by, the DNHP. For easy reference, the DNHP has been provided as Appendix A to this letter.

This letter has been updated based upon our meeting on December 6, 2017.

1. General

This project consists of four building (Buildings A, B, C, and D). The following is a summary of the buildings proposed for this development. Please see Appendix B to this letter for the proposed project site plan:

- Building A:
 - o Use Dialysis clinic
 - o Gross Area 10,345ft²
 - o Height 1-story
 - o Distance to Pipeline 300ft.
- Building B:
 - o Use Medical office building
 - o Gross Area 10,000ft²
 - o Height 1-story
 - o Distance to Pipeline 315ft.
- Building C:
 - o Use Professional office building
 - o Gross Area -5,000ft²
 - o Height 1-story
 - o Distance to Pipeline 205ft.
- Building D:
 - o Use Professional office building
 - \circ Gross Area -7,000ft²
 - o Height 1-story
 - o Distance to Pipeline 280ft.

The DNHP, Paragraph B, limits the proximity of new buildings to hazardous pipelines. Facilities that house occupants that are considered "requiring evacuation assistance" per A.4 of the DNHP are not permitted to be constructed within 500 feet of pipelines. No new structure is to be constructed within 200 feet of a

January 29, 2018 Page 2 of 4

Development Near A Hazardous Pipeline Ordinance Compliance

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

pipeline per DNHP, Paragraph C. As noted above, only Building A and B are proposed to conflict with these charging statements. Therefore, only Buildings A and B must comply with alternative provisions provided by the DNHP. However, due to concerns over future use of all buildings on the property, all buildings are included in the engineering evaluation to identify any potential future concerns.

2. DNHP, Paragraph B

Paragraph B of the DNHP begins by stating that no development of buildings within 500 feet of a hazardous pipeline shall be permitted where the building is used for the occupancy of those requiring evacuation assistance. The next sentence in Paragraph B provides an exception to this statement for such buildings between 200 and 500 feet of a pipeline, when Sections B.1 through B.3 are satisfied. The following sections of this report describe how this project satisfies Sections B.1 through B.3.

2.1. DNHP, Section B.1

Section B.1 requires that a performance based design be provided for each structure that proves an adequate time period for occupant evacuation to a safe place is available in the event of a pipeline leak or fire associated with the pipeline, after considering multiple factors. Each factor, and how the subject development complies, is described below.

2.1.1. Section B.1.a

Section B.1.a requires that the performance based design consider the requirements of Chapter 25-12, Article 7 (Uniform Fire Code) and the 2000 edition of the National Fire Protection Association 101 Life Safety Code.

Resolution: This project will comply with all regulations of the City of Austin Fire Code (2015 International Fire Code). FPCG's Fire Hazard Analysis and Fire Modeling Report cover the requirements of fire scenario selection based upon the 2015 NFPA 101, Life Safety Code, which is the most current edition of NFPA 101. FPCG's Fire Modeling Report is attached to this letter as Appendix D.

2.1.2. Section B.1.b

Section B.1.b requires that the performance based design consider the site and structure design.

Resolution: The fire modeling evaluation performed by FPCG evaluates the actual location of the pipeline, two possible worst-case fire locations, and the proposed location, size, and structure design for each of the buildings on-site.

2.1.3. Section B.1.c

Section B.1.c requires that the performance based design consider the structure's building materials.

Resolution: The fire modeling evaluation performed by FPCG considers the building materials in the conclusions. Should the results have shown temperature or heat flux values consistent with material ignition, recommendations for alternative materials could have been made. Since the fire modeling results indicate that said values are below those required for ignition of the proposed building materials, no modification to the current design is required.

2.1.4. Section B.1.d

Section B.1.d requires that the performance based design consider the structure's distance from the pipeline.

Resolution: The fire modeling evaluation performed by FPCG evaluates the actual location of the pipeline, two possible worst-case fire locations, and the proposed location, size, and structure design for each of the buildings on-site.

2.1.5. Section B.1.e

Section B.1.e requires that the performance based design consider the use of radiant energy barriers.

January 29, 2018 Page 3 of 4

Development Near A Hazardous Pipeline Ordinance Compliance

31 Deerfield Tract
Deer Lane and Brodie Lane

Austin, Texas

Resolution: When a fire produces enough radiant heat, or should flames impinge on a structure, radiant energy barriers can provide adequate protection by impeding the line-of-sight from the fire source to the target building. The fire modeling evaluation performed by FPCG evaluates the actual location of the pipeline fire scenarios with respect to each structure. Should the results have shown temperature or heat flux values consistent with building material ignition, inclusion of radiant energy barriers would have been made as part of the performance based design. Since the fire modeling results indicate that said values are below those required for ignition of the proposed building materials, no modification to the current design is required.

2.1.6. Section B.1.f

Section B.1.f requires that the performance based design consider access to the site and structure by emergency responders.

Resolution: Access to the site is provided by a looped fire lane with access to several on-site fire hydrants along the fire lane. One side of the fire lane loop is located north of the buildings, on the opposite side than the pipelines. The fire modeling results indicate that there is little to no difference in temperature or radiant heat flux to the north side of the structures, which indicates that there will be no issues accessing the fire lane and hydrants to the north during an event.

2.1.1.Section B.1.g

Section B.1.g requires that the performance based design consider available on-site resources for emergency responders.

Resolution: Access to the site is provided by a looped fire lane with access to several on-site fire hydrants along the fire lane. There are no additional on-site resources required, beyond those required by the City of Austin Fire Code, as a result of this analysis.

2.1.2. Section B.1.h

Section B.1.h requires that the performance based design consider the site topography and other natural features.

Resolution: The site slopes slightly down from the pipelines to the subject buildings by only a few feet. Because the pipelines carry liquified gaseous fuel which is buoyant upon release and vaporization, slope of the site does not factor into the fire scenario evaluation. Had a liquid fuel pipeline been present, a pool fire would have been evaluated. No other site natural features are present that could alter or affect the performance based design.

2.1.3. Section B.1.i

Section B.1.i requires that the performance based design consider the use of the structure.

Resolution: Section 1 of this report provides a description of the use of each on-site structure. All buildings are considered low-hazard uses as they are primarily for office use and out-patient medical care. There are no significant hazardous materials, no manufacturing, and no hazardous production processes housed in any of the proposed buildings. Use of the proposed structures does not affect this performance based design.

2.1.1.Section B.1.i

Section B.1.j requires that the performance based design consider the evacuation capability of the occupants.

Resolution: Because Paragraph B of the DNHP requires the performance based design prove adequate egress time is provided for building occupants, the evaluation capability, and therefore, evacuation speed of occupants, is imperative to be included in the analysis. Fire modeling is used to show what is called Available Safe Egress Time (ASET) by indicating the point in time in which the fire has grown to a point where a space or required egress path is no longer tenable. Tenability limits are defined by this project in the Acceptance Criteria document provided by FPCG. Once the ASET is identified, the Required Safe

January 29, 2018 Page 4 of 4

Development Near A Hazardous Pipeline Ordinance Compliance

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Egress Time (RSET) is calculated by factoring in the evacuation speed of the subject population. A design option is successful when the ASET value is greater than the RSET value.

Because the fire modeling for this project shows that the tenability limits are never reached (the site evacuation routes always remain tenable, assuming FPCG's recommendations for Building C are followed), the ASET value is effectively infinite. Therefore, the RSET value does not need to be calculated to ensure ASET exceeds RSET.

2.2. DNHP, Section B.2

Section B.2 requires that the structure incorporate a system for the early detection and notification of a pipeline leak, if the fire chief determines that an appropriate system is commercially available.

Resolution: FPCG has designed a gas detection system for the development that incorporates propane gas detectors located immediately adjacent to the pipeline easement as well as audible and visible beacons mounted in line with the detectors as well as at the subject buildings. Please see Appendix C to this letter for details.

2.3. DNHP, Section B.3

Section B.3 requires that the performance-based design for occupant evacuation and the early detection and notification system are certified and sealed by an engineer registered in Texas.

Resolution: FPCG is a licensed engineering firm in Texas. Our firm number is F-15865. One of our licensed engineers will be responsible for, and will sign and seal the system design. Modifications to the original design are attached here, based upon AFD feedback.

As there are no further requirements associated with the DNHP, this concludes our letter. In closing, FPCG has confirmed that the subject property complies with the DNHP and should be granted permission by the City of Austin to develop in the manner described herein and depicted in the attachments to this letter.

If you have any questions, please do not hesitate to contact me by phone at (210) 858-2389 or by e-mail to gilead@firepcg.com.

Sincerely yours,

Gilead R. Ziemba, P.E., M

Partner & Sr. Fire Protection Eng.

Attachments: Appendix A - Development Near a Hazardous Pipeline (§25-2-516 Austin Code of

Ordinances)

Appendix B – 31 Deerfield Tract Proposed Site Plan

Appendix C – Early Detection and Warning System Design Drawings (REV 1)

Appendix D – 17-065 31Deerfield - Fire Modeling Report r2

January 29, 2018 APPENDICES **Development Near A Hazardous Pipeline Ordinance Compliance – Revision 1**

31 Deerfield Tract
Deer Lane and Brodie Lane
Austin, Texas

Appendix A

Development Near a Hazardous Pipeline (§25-2-516 Austin Code of Ordinances)

§ 25-2-516 - DEVELOPMENT NEAR A HAZARDOUS PIPELINE.

(A) In this section:

- (1) HAZARDOUS PIPELINE means a pipeline designed for the transmission of a "hazardous liquid", as defined by Title 49, Code of Federal Regulations, Section 195.2, with an inside diameter of eight inches or more.
- (2) NEW CONSTRUCTION means the construction after April 20, 2003 of a structure intended for human occupancy, and includes the construction of a new structure, the construction of an addition to an existing structure and the reconstruction of a portion of an existing structure. The term excludes an addition to or the reconstruction or replacement of a structure existing on April 21, 2003 used for:
 - (a) single-family residential use;
 - (b) small lot single-family residential use;
 - (c) single-family attached residential use;
 - (d) duplex residential use;
 - (e) two-family residential use;
 - (f) mobile home residential use; or
 - (g) in a neighborhood plan combining district:
 - (i) cottage special use;
 - (ii) urban home special use; or
 - (iii) secondary apartment special use.
- (3) RESTRICTED PIPELINE AREA includes an area within 25 feet of a hazardous pipeline and an area within a hazardous pipeline easement.
- (4) USE REQUIRING EVACUATION ASSISTANCE includes the following uses:
 - (a) congregate living;
 - (b) convalescent services;
 - (c) detention facilities;
 - (d) day care services (commercial);
 - (e) hospital (general);
 - (f) hospital (limited);
 - (g) medical offices exceeding 5,000 square feet of gross floor area;
 - (h) private primary educational facilities;
 - (i) private secondary educational facilities;
 - (i) public primary educational facilities;
 - (k) public secondary educational facilities; and
 - (l) retirement housing (large site).

- (B) A use requiring evacuation assistance is prohibited in a structure intended for human occupancy that is located within 500 feet of a hazardous pipeline. This prohibition does not apply to a structure that is located between 200 and 500 feet of a hazardous pipeline if by resolution the council determines, after receiving a recommendation from the fire chief, that:
 - (1) the structure has a performance-based design that provides an adequate time period for occupant evacuation to a safe place in the event of a pipeline leak or fire associated with the pipeline, after considering:
 - (a) the requirements of <u>Chapter 25-12</u>, Article 7 (*Uniform Fire Code*) and the 2000 edition of the National Fire Protection Association 101 Life Safety Code;
 - (b) the site and structure design;
 - (c) the structure's building materials;
 - (d) the structure's distance from the pipeline;
 - (e) the use of radiant energy barriers;
 - (f) access to the site and the structure by emergency responders;
 - (g) available on-site resources for emergency responders;
 - (h) the topography and other natural features;
 - (i) the use of the structure; and
 - (j) the evacuation capability of the occupants;
 - (2) the structure incorporates a system for the early detection and notification of a pipeline leak, if the fire chief determines that an appropriate system is commercially available; and
 - (3) the performance-based design for occupant evacuation and the early detection and notification system are certified and sealed by an engineer registered in Texas.
- (C) A person may not build new construction within 200 feet of a hazardous pipeline unless:
 - (1) the fire chief determines that:
 - (a) the new construction has a performance-based design that provides a minimum one-hour time period for occupant evacuation to a safe place in the event of a pipeline leak or a fire associated with the pipeline, in accordance with <u>Chapter 25-12</u>, Article 7 (*Uniform Fire Code*) or the 2000 edition of the National Fire Protection Association 101 Life Safety Code;
 - (b) the new construction incorporates a system for the early detection and notification of a pipeline leak, if the fire chief determines that an appropriate system is commercially available; and
 - (c) the performance-based design for occupant evacuation and the early detection and notification system are certified and sealed by an engineer registered in Texas; or
 - (2) the new construction complies with the standards for construction near a pipeline prescribed by the Fire Criteria Manual.
- (D) A person may not place a structure or excavate within a restricted pipeline area.

- (1) This prohibition does not apply to:
 - (a) the pipeline or an appurtenance;
 - (b) a facility that produces, consumes, processes, or stores the product transported by the pipeline, including a power generation facility;
 - (c) a utility line that crosses the restricted pipeline area, including an appurtenance to the line;
 - (d) a utility service connection;
 - (e) a road;
 - (f) a surface parking lot; or
 - (g) a structure or excavation that the director determines does not disturb the pipeline or impede its operation.
- (2) Before a person may place a road, surface parking lot, or utility line in a restricted pipeline area, the person must deliver to the director a certification by a registered engineer stating that the proposed construction activity and structure are designed to prevent disturbing the pipeline or impeding its operation.

Source: Ord. 030410-12; Ord. 031211-11.

January 29, 2018 APPENDICES

Development Near A Hazardous Pipeline Ordinance Compliance – Revision 1

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Appendix B

31 Deerfield Tract Proposed Site Plan

SP2017-0133C

January 29, 2018 APPENDICES

Development Near A Hazardous Pipeline Ordinance Compliance – Revision 1

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Appendix C

Early Detection and Warning System Design Drawings (REV 1)

EMERGENCY ALARM SYSTEM (EAS) — GENERAL NOTES

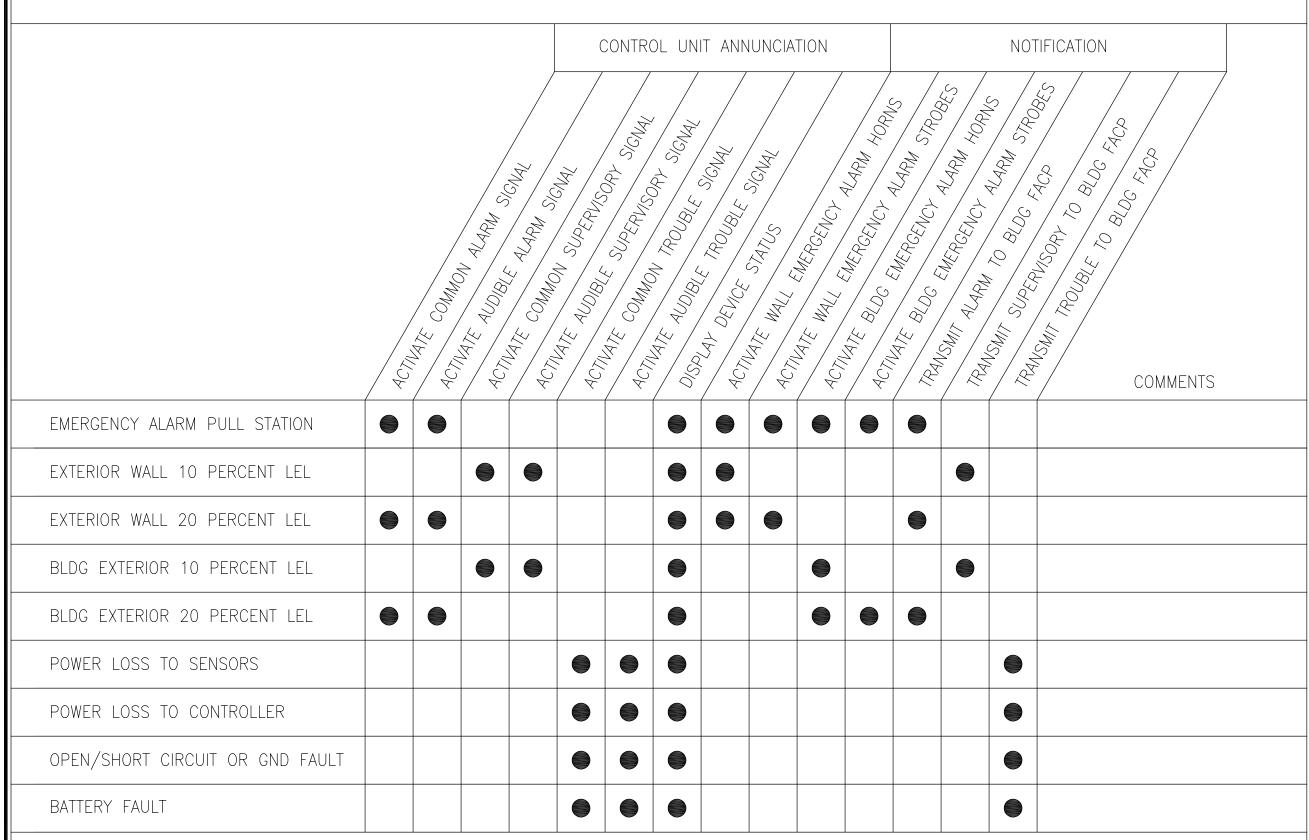
- 1. THESE DRAWINGS DEPICT GENERAL LOCATIONS OF LIFE SAFETY EQUIPMENT & FIELD DEVICES. EXACT ROUTING OF CONDUITS AND WIRE TO BE DETERMINED IN THE FIELD BY THE INSTALLING CONTRACTOR TO SUIT CONDITIONS. ALL CHANGES SHALL BE CLEARLY INDICATED ON THE RECORD DRAWINGS.
- 2. SHOULD ANY CONDITIONS EXIST THAT DIFFER FROM WHAT IS INDICATED ON THESE DRAWINGS WHICH CAUSE MAJOR DEVIATIONS IN THE WORK SHOWN, THE CONTRACTOR SHALL CONTACT FIRE PROTECTION CONSULTING GROUP, LLC IN A TIMELY MANNER SO AS NOT TO IMPAIR THE CONSTRUCTION SCHEDULE.
- 3. CONTRACTOR IS RESPONSIBLE FOR MAKING AND OBTAINING APPROVAL FOR ALL NECESSARY ADJUSTMENTS IN CIRCUITING AS REQUIRED TO ACCOMMODATE THE RELOCATION OF EQUIPMENT AND/OR DEVICES WHICH ARE AFFECTED BY ANY AUTHORIZED CHANGE. ALL CHANGES SHALL BE CLEARLY INDICATED ON THE RECORD DRAWINGS.
- 4. A STAMPED SET OF APPROVED EMERGENCY ALARM DRAWINGS SHALL BE AT THE JOB SITE AND SHALL BE USED FOR INSTALLATION.
- 5. THE POWER CIRCUIT TO THE EACP AND TO THE EMERGENCY ALARM POWER SUPPLIES SHALL BE ON A DEDICATED 120V, 20A BRANCH CIRCUIT BREAKER, AND SHALL HAVE A RED MARKING, LOCK—ON PROVISION AND SHALL BE IDENTIFIED AS "EMERGENCY ALARM CIRCUIT CONTROL." THE LOCATION OF THE CIRCUIT DISCONNECT MEANS
- (CIRCUIT BREAKER) SHALL BE PERMANENTLY IDENTIFIED AT THE EMERGENCY ALARM CONTROL UNIT.

 6. UPDATE THE AS-BUILT DRAWING SET DAILY WITH JOB PROGRESS. RETURN THE AS-BUILT DRAWING SET TO THE
- OWNER NO LATER THAN 7 DAYS AFTER FINAL TEST.

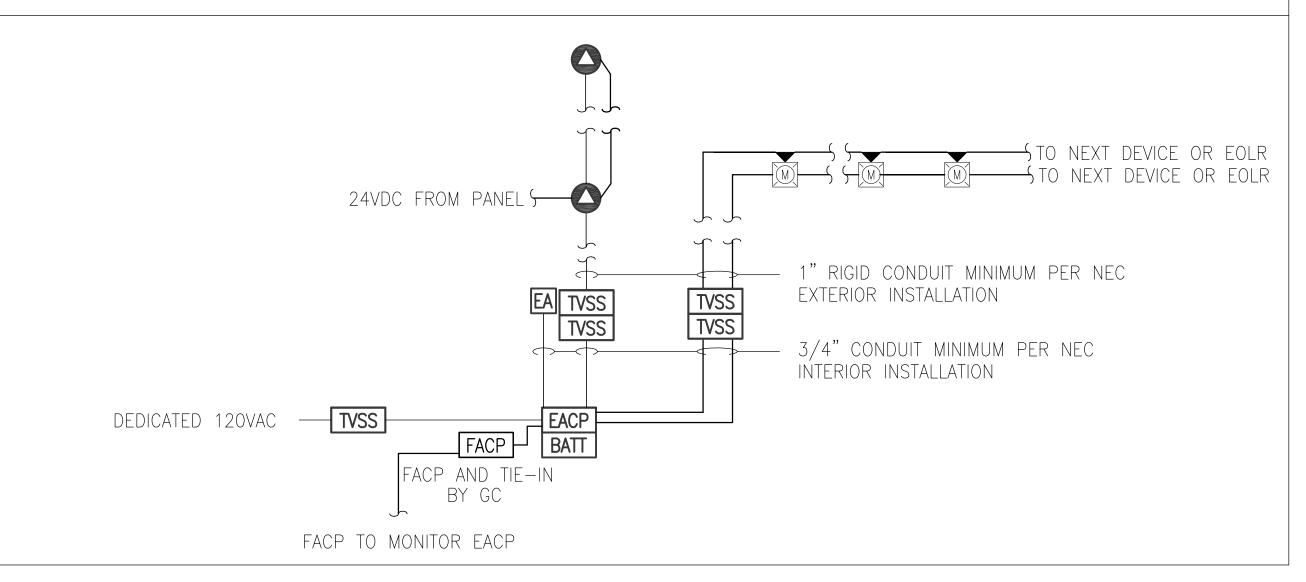
 7. THE CONTRACTOR WILL MAINTAIN ALL AREAS OF THE BUILDING IN A NEAT AND WORKMAN LIKE MANNER.
- 8. DO NOT APPLY POWER EXCEPT IN THE PRESENCE OF A FACTORY TRAINED TECHNICAL REPRESENTATIVE.
 9. THE EMERGENCY ALARM INSTALLER WILL MAINTAIN THE FIRE RESISTANCE INTEGRITY OF ALL WALL, CEILING, AND ROOF ASSEMBLIES ANY TIME THAT WORK IS NOT ACTIVELY BEING PERFORMED.
- 10. INSTALLATION OF DEVICES SHALL BE IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. POWER LIMITED AND NON-POWER LIMITED FIELD WIRING MUST BE INSTALLED WITHIN THE EACP ENCLOSURE IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS AND NEC.
- 11. ALL WIRING SHALL BE INSTALLED ACCORDING TO NFPA 70 (NEC).
- 12. EMERGENCY ALARM CIRCUITS SHALL BE IDENTIFIED IN ACCORDANCE WITH APPROPRIATE SECTION OF NEC 760.

 MARK ALL EMERGENCY ALARM WIRES IN ACCORDANCE WITH NEC 760 SECTIONS FOR POWER LIMITED AND NON-POWER LIMITED WIRE.
- 14 EMERGENCY ALARM CABLE INSTALLED IN DUCTS, PLENUM, AND OTHER SPACES USED FOR ENVIRONMENTAL AIR SHALL BE TYPE FPLP.
- 15. EMERGENCY ALARM CABLE INSTALLED IN UNDERGROUND CONDUIT OR OTHER WET LOCATIONS SHALL BE UL LISTED FOR WET LOCATIONS.
- 16. EMERGENCY ALARM CIRCUITS EXTENDING BEYOND ONE BUILDING AND RUN OUTDOOR SHALL BE INSTALLED IN ACCORDANCE WITH NFPA 70 ARTICLES 760, 770, 725 AND 800 WHERE APPLICABLE.
- 17. ALL WIRING, INCLUDING SHIELDS MUST BE DRY AND FREE OF SHORTS AND GROUNDS.
- 18. ALL SHIELDED WIRE MUST HAVE SHIELD CONTINUITY AT FULL LENGTH OF THE WIRE.
- 19. ONLY SYSTEM WIRING CAN BE RUN IN THE SAME CONDUIT.
- 20. 120VAC IS NOT PERMITTED IN THE SAME CONDUIT WITH LOW VOLTAGE WIRING.
- 21. MAINTAIN 40 PERCENT CONDUIT FILL RATIO AS PER NEC REQUIREMENTS.
- 22. VISUAL OR AUDIBLE/VISUAL MOUNTING TO BE 80" TO 96" IN FROM THE FINISHED FLOOR TO THE BOTTOM OF THE DEVICE PER NFPA 72.
- 23. AUDIBLE DEVICE MOUNTING TO BE A MINIMUM OF 90" FROM THE FINISHED FLOOR TO THE TOP OF DEVICE AND NO MORE THAN 6" FROM TOP OF DEVICE TO CEILING PER N.F.P.A. 72.
- 24. MANUAL PULL STATION SHALL BE NOT LESS THAN 42" AND NOT MORE THAN 48" FROM OPERABLE PART OF DEVICE TO FLOOR LEVEL PER N.F.P.A. 72.

SEQUENCE OF OPERATION



EAS RISER — DIAGRAMMATIC PURPOSES ONLY



SYMBOL KEY

Emergency Alarm Notification

Horn/Strobe — 4—Wire — Amber 110 CD — Weatherproof

Gas Detection Symbols

Gas Detector Sensor — Weatherproof HONEYWELL Sensepoint XCD IR Methane % LEL Sunshade Accessory

<u>Manual Devices</u>

EA Emergency Alarm Push—Pull Station

<u>Control Panels</u>

ACP Emergency Alarm/BAS Interface Panel

BATT Battery Cabinet

/SS Transient Voltage Surge Suppressor

Suggested Conduit Route



1) PUSH-PULL STATION

NTS

Sensepoint XCD comprises of the main parts as shown below.

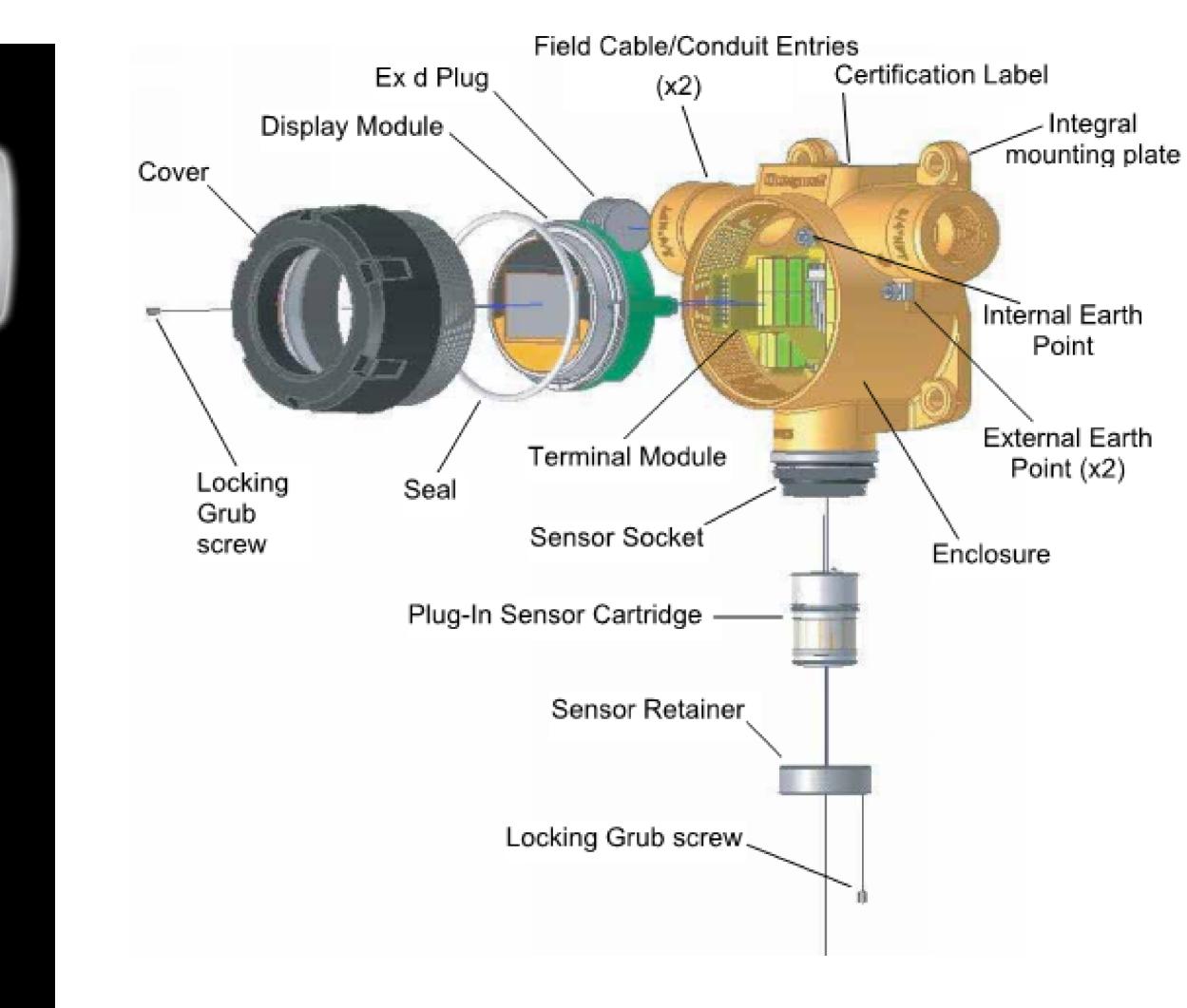
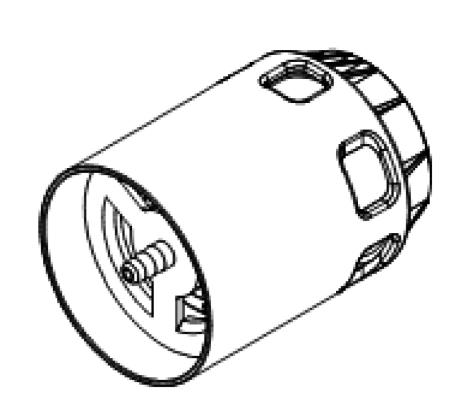


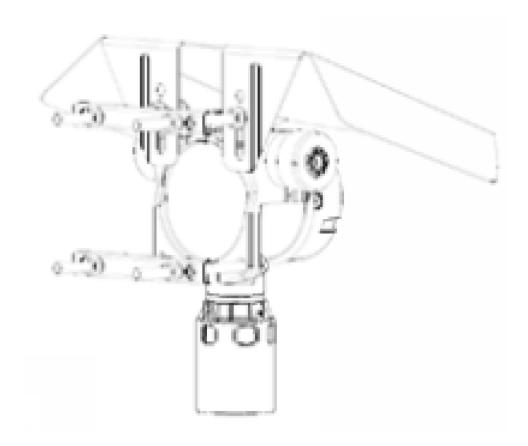
Diagram 1. - Exploded View



200

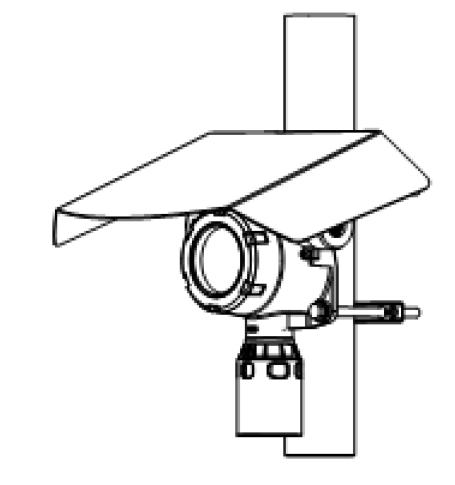
Standard Weather Protection

The Standard Weather Protection (P/N: SPXCDWP) is designed to protect the sensor from changes in environmental conditions. This is recommended to be fitted to a Sensepoint XCD sensor for outdoor exposed applications, (supplied with XCD kit).



Sunshade Deluge Cover

The XCD Sunshade Deluge Cover (P/N: SPXCDSDP) is an optional accessory that may be fitted to the integral mounting plate. This accessory is designed to protect XCD from overheating in exposed hot and arid climates, particularly offering additional protection from thermal shock in Tropical Environments



Typical Mounting Arrangement



NOT FOR REGULATORY APPROVAL, PERMITTING OR CONSTRUCTION

FIRE PROTECTION ENGINEER
FIRE PROTECTION CONSULTING GROUP, LC
339 SANDALWOOD LANE
SAN ANTONIO, TX 78216
210.858.2389 MAIN
Texas Firm No. F-15865

PROJECT OWNER

5 CONGRESS JITE 1515 JSTIN, TEKAS 78701 vw.practicerealestategroup.com



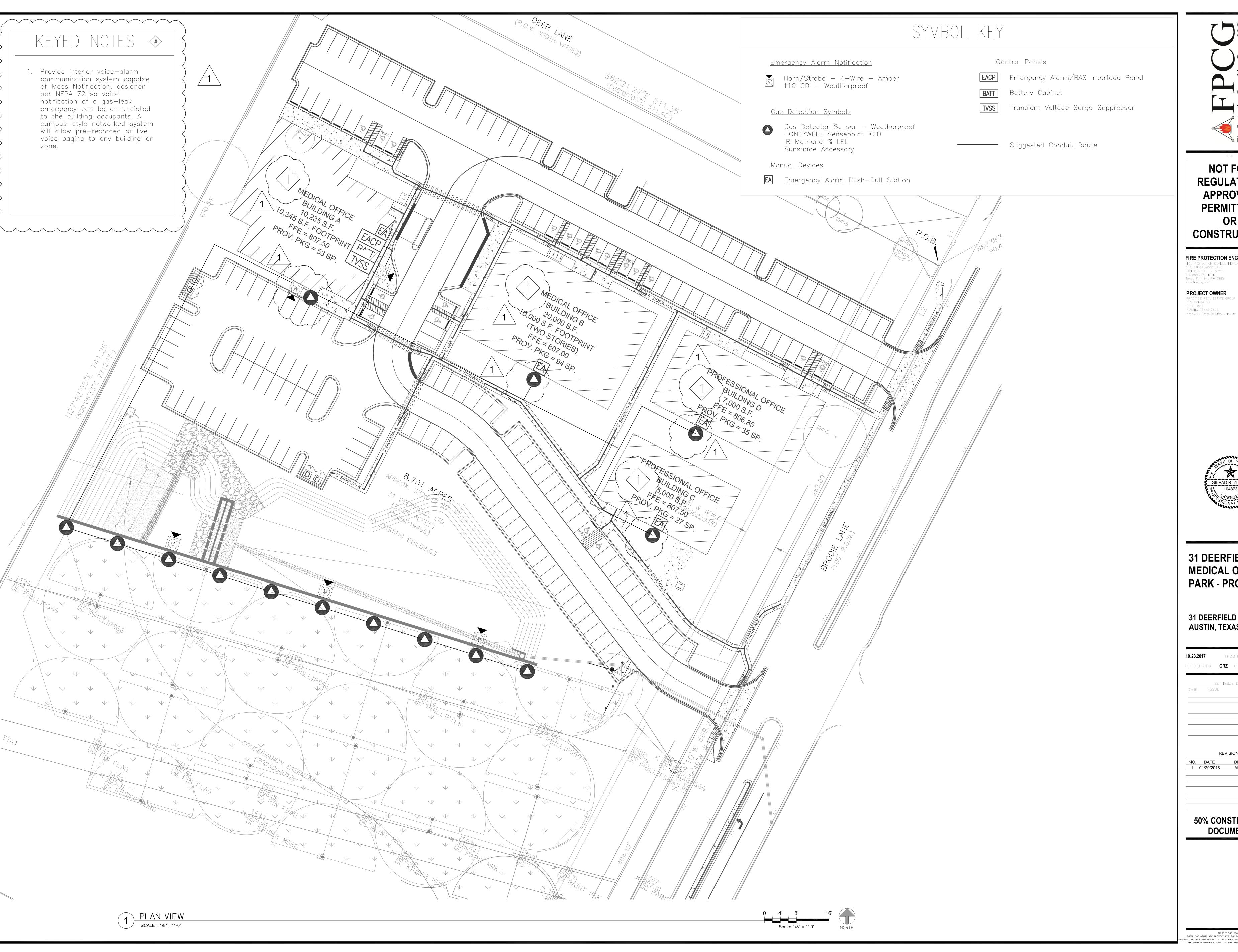
31 DEERFIELD
MEDICAL OFFICE
PARK - PROPOSED

31 DEERFIELD AUSTIN, TEXAS

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FOR REVIEW - NOT FOR CONSTRUCTION

2 GAS DETECTOR AND RECOMMENDED ACCESSORIES





NOT FOR REGULATORY APPROVAL, **PERMITTING** CONSTRUCTION

FIRE PROTECTION ENGINEER

FIRE PROTECTION CONSULTING GROUP, L.C

339 SANDALWOOD LANE

SAN ANTONIO, TX 78216

210.858.2389 MAIN

Texas Firm No. F-15865

www.firepog.com



31 DEERFIELD **MEDICAL OFFICE PARK - PROPOSED**

31 DEERFIELD **AUSTIN, TEXAS**

50% CONSTRUCTION DOCUMENTS

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January 29, 2018 APPENDICES

Development Near A Hazardous Pipeline Ordinance Compliance – Revision 1

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Appendix D

17-065 31Deerfield - Fire Modeling Report_r2

FIRE MODELING REPORT

Project Information:

31 Deerfield Tract Austin, Texas

Prepared For:

Practice Real Estate Group 515 Congress, Suite 1515 Austin, Texas 78701





339 Sandalwood Lane San Antonio, Texas 78216 www.FIREpcg.com Main Office +1 210.858.2389



Table of Contents

Purpose and Scope	
Executive Summary	
List of Documents Reviewed	
Applicable Codes and Standards	
1. Hazard Analysis Summary	
2. Fire Modeling Software	
2.1. Selection of Model Type	
2.2. Fire Dynamics Simulator	
3. Fire Modeling Results	
3.1. Project Fire Scenario #2 – Propane Jet Fire	
3.1.1. PFS #2 Modeling Results – With Wind	
4. Comparison of Results to Egress Time	
5. Conclusions	



Table of Figures

Figure 1: CAD model screen shot	∠
Figure 2: HRR curve used for PFS 2 fire modeling	5
Figure 3: Annualized wind-rose provided by TCEQ for Austin, Texas.	5
Figure 9: PFS-2 Wind, Z=2.0m, CO2 at 3 seconds.	
Figure 10: PFS-2 Wind, Z=2.0m, CO2 at 54 seconds.	8
Figure 11: PFS-2 Wind, Z=2.0m, CO2 at 102 seconds	9
Figure 12: PFS-2 Wind, Z=2.0m, CO2 at 201 seconds	10
Figure 13: PFS-2 Wind, Z=2.0m, CO2 at 300 seconds	
Figure 14: PFS-2 Wind, Z=2.0m, CO at 3 seconds.	
Figure 15: PFS-2 Wind, Z=2.0m, CO at 102 seconds.	
Figure 16: PFS-2 Wind, Z=2.0m, CO at 300 seconds.	14
Figure 17: PFS-2 Wind, Z=2.0m, O2 at 3 seconds	
Figure 18: PFS-2 Wind, Z=2.0m, O2 at 102 seconds	16
Figure 19: PFS-2 Wind, Z=2.0m, O2 at 300 seconds.	17
Figure 20: PFS-2 Wind, Z=2.0m, Temperature at 3 seconds	18
Figure 21: PFS-2 Wind, Z=2.0m, Temperature at 18 seconds	19
Figure 22: PFS-2 Wind, Z=2.0m, Temperature at 30 seconds	20
Figure 23: PFS-2 Wind, Z=2.0m, Temperature at 60 seconds	21
Figure 24: PFS-2 Wind, Z=2.0m, Temperature 120 seconds.	22
Figure 25: PFS-2 Wind, Z=2.0m, Temperature 240 seconds.	23
Figure 26: PFS-2 Wind, Z=2.0m, Temperature 300 seconds.	24

Via e-mail to: trac@practicerealestategroup.com



January 29, 2018

Mr. Trac Bledsoe Practice Real Estate Group 515 Congress, Suite 1515 Austin, Texas 78701

RE: Fire Modeling Report – Revision 2

31 Deerfield Austin, Texas

Dear Mr. Bledsoe:

Thank you for contacting Fire Protection Consulting Group, LLC (FPCG) regarding this project. In conclusion to the overall egress study and performance based design performed by FPCG, this report is being provided to gain acceptance of the proposed acceptance criteria to be used in the forthcoming evaluation of the 31 Deerfield Tract proposed Dialysis Clinic.

Additional fire modeling screen shots are available via the hyperlinks in Attachment D to this report.

Purpose and Scope

The purpose of this report is to evaluate the hazard calculations and/or building fire models as part of the performance based analysis of the facility. This report addresses the follow topics:

• Fire Modeling Report – FPCG has developed and evaluated computational fluid dynamics computer simulations to compare each Project Fire Scenario (PFS) identified in the project Hazard Analysis with the results of the Acceptance Criteria to determine if the site egress paths remain tenable for the amount of time required for site evacuation. This report summarizes our development, findings, and conclusions of said fire modeling.

Executive Summary

FPCG has developed and evaluated computational fluid dynamics computer simulations to compare each Project Fire Scenario (PFS) identified in the project Hazard Analysis. FPCG anticipates that a release of liquified propane will result in a highly buoyant vapor cloud formation, therefore would result in an explosion or fire ball rather than a sustained fire event. As explosion scenarios are excluded from this evaluation, FPCG has evaluated the likely sustained fire event following an explosion or fire ball event, which would be an ignited pressurized plume release of propane resulting in a very strong jet fire.

FPCG's calculations anticipate flame length over 70 meters long, which will extend towards the development in a cross-wind condition. Propane has three times the amount of carbon atoms per mole, and will therefore produce significantly more radiative energy, which is the expected worst-case heat transfer mode for jet flames that do not impinge on a target.

The results with the prevailing wind are presented in the report by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire event. Each result includes a color bar to the right of the screen shot with a black band to indicate the location of the pass/fail point for each tenability criteria. The models were run for a total of five minutes (300seconds), after which equilibrium is reached. Additional run time will not change the results, and was therefore not necessary for criteria evaluation.

The results in the Fire Modeling Report show no signs of reaching the tenability threshold near the subject buildings at the equilibrium state, except for Building C, which reaches the heat flux tenability limit at the south face of the building only. For this reason FPCG recommends that all egress points from Buildign C be provided from the northern face of the building. For all other buildings, the tenability is never reached.

January 29, 2018 Page 3 of 26

Fire Modeling Report – Revision 2

31 Deerfield Tract

Austin, Texas

Because of this, it can be stated that regardless of the time needed for egress, egress movement will not be challenged by the anticipated fire event.

List of Documents Reviewed

The following is a list of documents received from your office that were reviewed or otherwise used in the preparation of this report:

- 31 Deerfield Grading & Utilities Exhibit.pdf
- GasLineLocMap.pdf

If any of these documents have changed from the version noted above, please contact our office to determine if the modification affects the results of this analysis and report.

Applicable Codes and Standards

The following codes and standards have been referenced and utilized during this analysis and form the basis for this report:

- Austin Code of Ordinance §25-2-516, Development Near A Hazardous Pipeline (ACO)
- 2015 edition of the International Building Code (IBC), as adopted by the City of Austin
- 2015 edition of the International Fire Code (IFC), as adopted by the City of Austin
- 2015 edition of NFPA 101, Life Safety Code (LSC), as adopted by the Texas State Fire Marshal's Office

1. Hazard Analysis Summary

The results of the Hazard Analysis identified the following PFS's as needing to proceed to the modeling stage of the project. See the associated Appendix to this report for a full description of each PFS:

• PFS-2: FPCG anticipates that a release of liquified propane will result in a highly buoyant vapor cloud formation, therefore would result in an explosion or fire ball rather than a sustained fire event. As explosion scenarios are excluded from this evaluation, FPCG will evaluate the likely sustained fire event following an explosion or fire ball event, which would be an ignited pressurized plume release of propane resulting in a very strong jet fire.

The remaining sections of this report will identify the results of said fire modeling.

2. Fire Modeling Software

The following sections describe the selection method of the fire modeling used to evaluate each PFS identified by the Hazard Analysis.

2.1. Selection of Model Type

To begin the modeling phase, multiple types of models were considered. The building, fire type, and necessary results were contemplated when selecting the appropriate fire model type. Due to the complex fire geometry (tilted jet flame deflected by high wind conditions), the need to evaluate an incident wind speed and off-axis direction, the need to evaluate total heat flux to model surfaces, and the need to determine species concentration to evaluate the project tenability criteria led to the selection of a Computational Fluid Dynamics (CFD) model type.

2.2. Fire Dynamics Simulator

Fire Dynamic Simulator (FDS) version 6.1.2 was selected for this project. It is a CFD model developed by the National Institute of Standards and Technology (NIST) along with many independent collaborators, researchers, and beta testers in the pursuit of the an open-source and robust software that is routinely validated by full-scale fire testing for various scenarios. FDS is a model of fire-driven fluid flow. The software solves numerically a form of the Navier-Stokes equations appropriate for low-speed, thermally-

January 29, 2018 Page 4 of 26

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

driven flow, with an emphasis on smoke and heat transport from fires. NIST has also developed a viewing software called Smokeview which is a visualization program that is used to display the output of FDS simulation. By using both FDS and Smokeview, FPCG is able to compute the complex fire scenarios and report visual confirmation of the results.¹

The following computer screen shot, looking from the northwest to the southwest direction, shows the modeled building structure used for this evaluation.

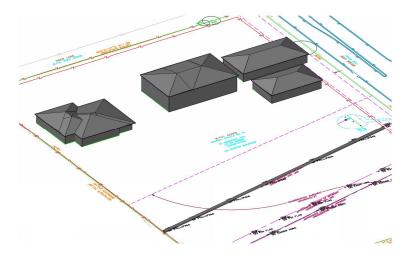


Figure 1: CAD model screen shot.

3. Fire Modeling Results

The following sections describe the results of the fire modeling performed to evaluate the PFS identified by the Hazard Analysis. All models were evaluated for the following tenability criteria at an elevation of 2 meters above finished-grade as this is the approximate height of a person's head above each of the egress path walking surfaces leading from the building to the public way.

Building C is the closest building to the a hazardous pipeline, therefore additional fire modeling was performed, and reported in Appendix D which moved the fire in-line with the closest point of Building C.

3.1. Project Fire Scenario #2 – Propane Jet Fire

FPCG's calculations anticipate flame length over 70 meters long, which will extend towards the development in a cross-wind condition. Though very similar to PFS-3, propane has three times the amount of carbon atoms per mole, and will therefore produce significantly more radiative energy, which is the expected worst-case heat transfer mode for jet flames that do not impinge on a target. For these reasons, FPCG has included this scenario for further evaluation.

¹ http://www.nist.gov/el/fire research/fds smokeview.cfm

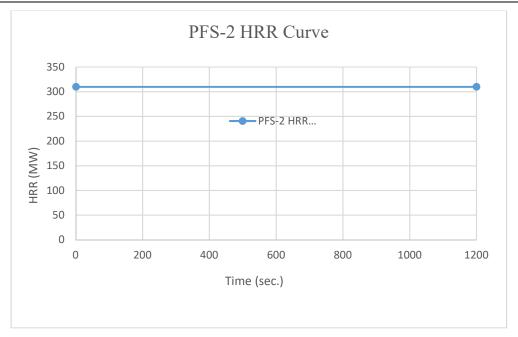


Figure 2: HRR curve used for PFS 2 fire modeling.

3.1.1.PFS #2 Modeling Results – With Wind

Because the Fire Scenario is open to the environment, FPCG has provided modeling to identify the anticipated results based upon an average design wind velocity from the prevailing wind direction.

Based upon data provided by the Texas Commission on Environmental Quality (TCEQ), represented as wind speed and direction information in Figure 3 below, the prevailing wind direction for this project is a south-easterly wind with an average speed of 20 knots or 10.3 meters per second.

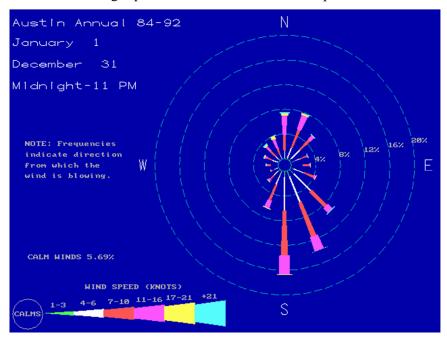


Figure 3: Annualized wind-rose provided by TCEQ for Austin, Texas.

The results of PFS-2 with the prevailing wind are presented below by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire development. Each result includes a color bar to the right of the screen shot with a black band to indicate the location of the

January 29, 2018 Page 6 of 26

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

pass/fail point for each tenability criteria. The models were run for a total of five minutes (300seconds), after which equilibrium is reached. Additional run time will not change the results, and was therefore not necessary for criteria evaluation.

3.1.1.1. Heat Flux

The results indicating heat flux (2.5kW/m² maximum) are presented at the hyperlinks provided in Appendix D to this report. The links include several screen shots of the Smokeview visualization software output at multiple points in time during the fire development. The hyperlinks are also provided here for reference.

Jet Fire – Building C Aligned:

• Net Heat Flux https://www.dropbox.com/sh/6j3h9bxlwuko1h9/AAApFS1oQZycD5sbGYxiYmBTa?dl=0

Jet Fire - South:

Net Heat Flux
https://www.dropbox.com/sh/8j2o0rzi87dyrby/AACbkTel_oDqb-G3z-TxpNAfa?dl=0

Jet Fire - North:

Net Heat Flux https://www.dropbox.com/sh/i5309604a9f77vt/AADZXoxatlGwWK-f9CO7tZ3qa?dl=0

Austin, Texas

3.1.1.2. Carbon Dioxide Volume Fraction

The results indicating carbon dioxide concentration (4% maximum) are presented below by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire development.

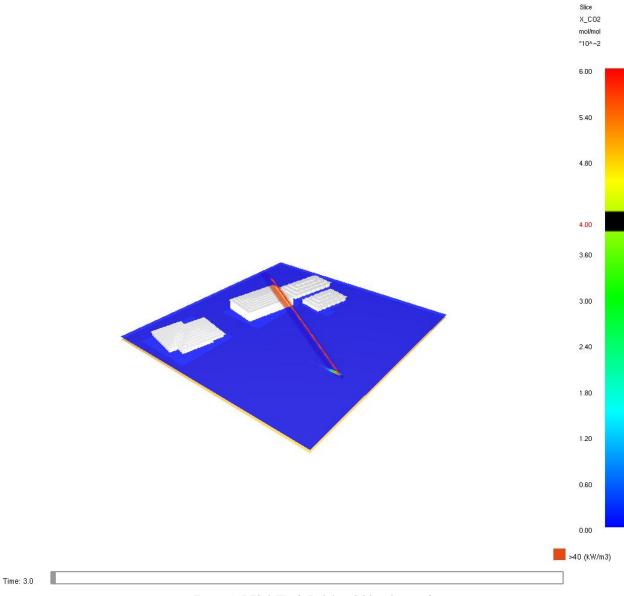


Figure 4: PFS-2 Wind, Z=2.0m, CO2 at 3 seconds.

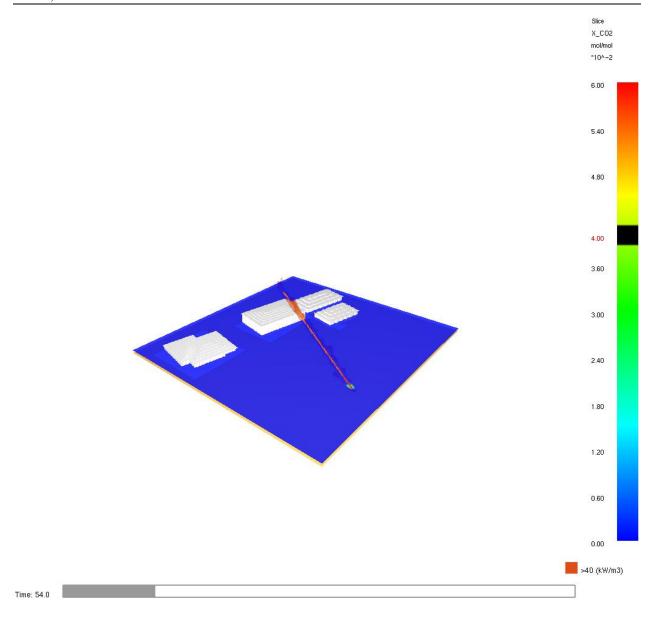


Figure 5: PFS-2 Wind, Z=2.0m, CO2 at 54 seconds.

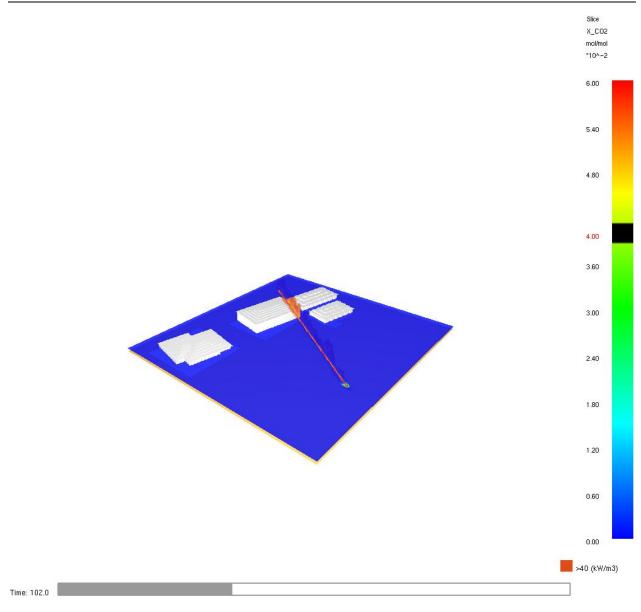


Figure 6: PFS-2 Wind, Z=2.0m, CO2 at 102 seconds.

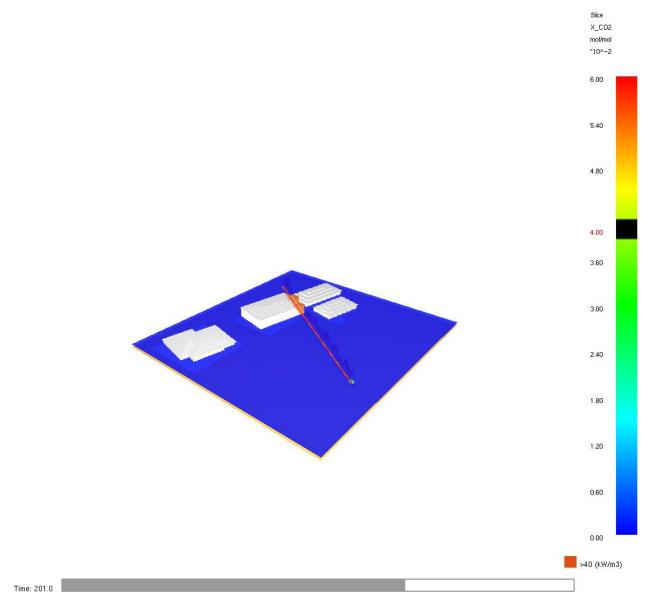


Figure 7: PFS-2 Wind, Z=2.0m, CO2 at 201 seconds.

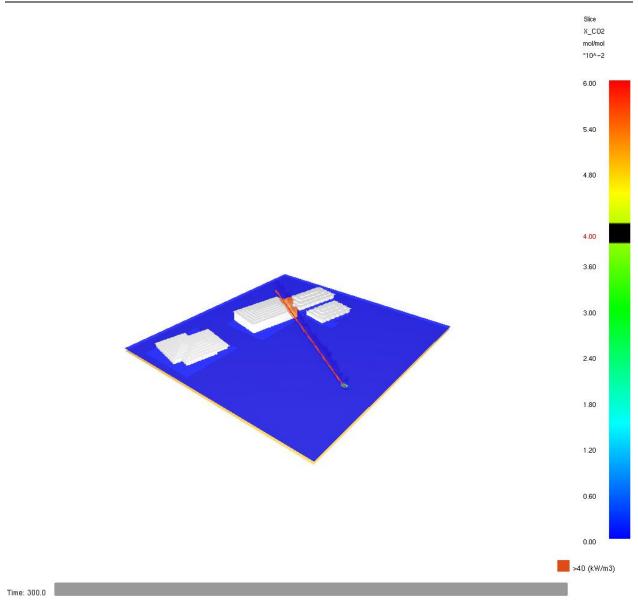


Figure 8: PFS-2 Wind, Z=2.0m, CO2 at 300 seconds.

3.1.1.3. Carbon Monoxide Volume Fraction

The results indicating carbon monoxide concentration (1200ppm maximum) are presented below by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire development.

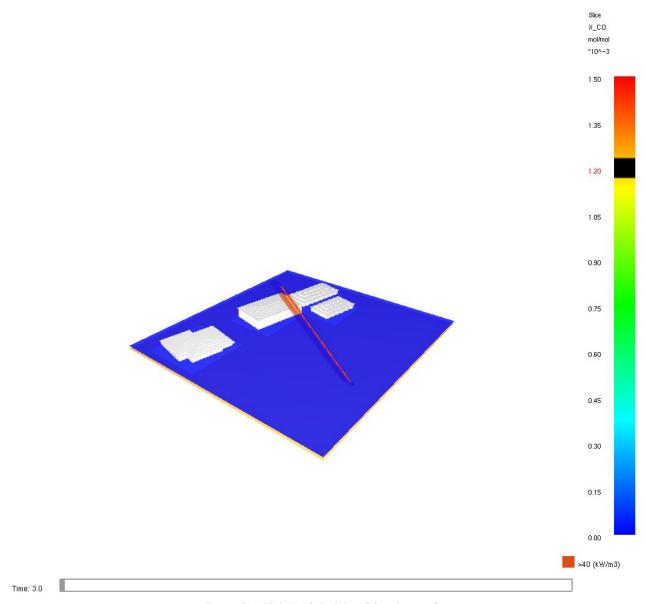


Figure 9: PFS-2 Wind, Z=2.0m, CO at 3 seconds.

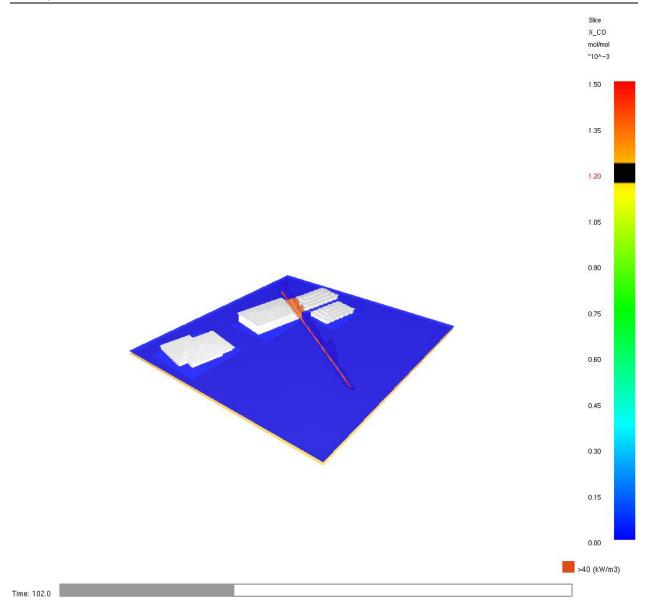


Figure 10: PFS-2 Wind, Z=2.0m, CO at 102 seconds.

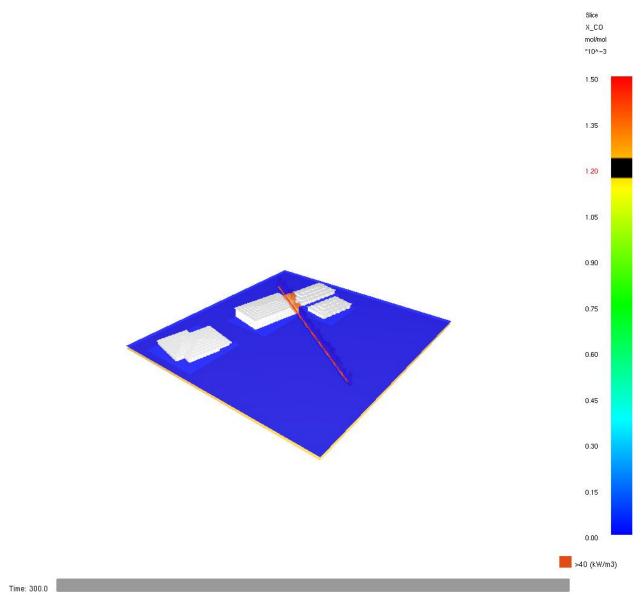


Figure 11: PFS-2 Wind, Z=2.0m, CO at 300 seconds.

3.1.1.4. Oxygen Concentration

The results indicating oxygen concentration (15% minimum) are presented below by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire development.

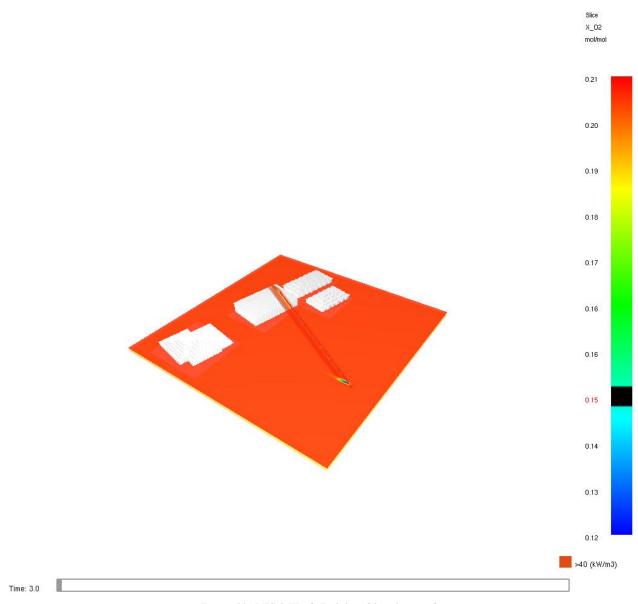


Figure 12: PFS-2 Wind, Z=2.0m, O2 at 3 seconds.

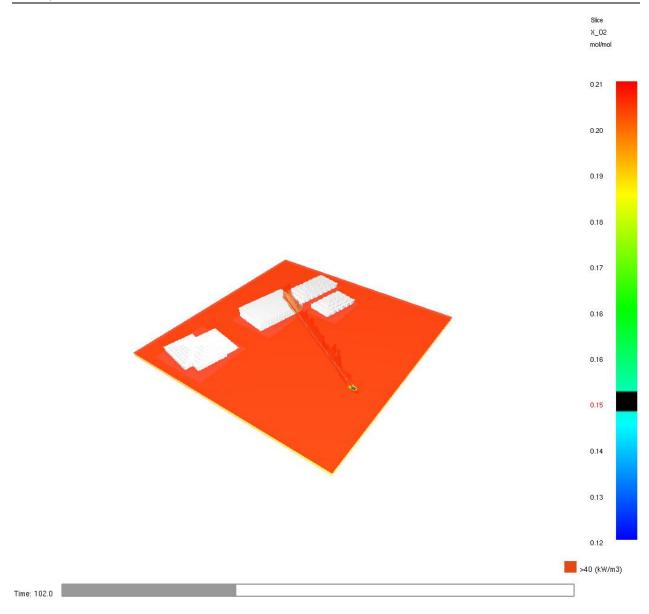


Figure 13: PFS-2 Wind, Z=2.0m, O2 at 102 seconds.

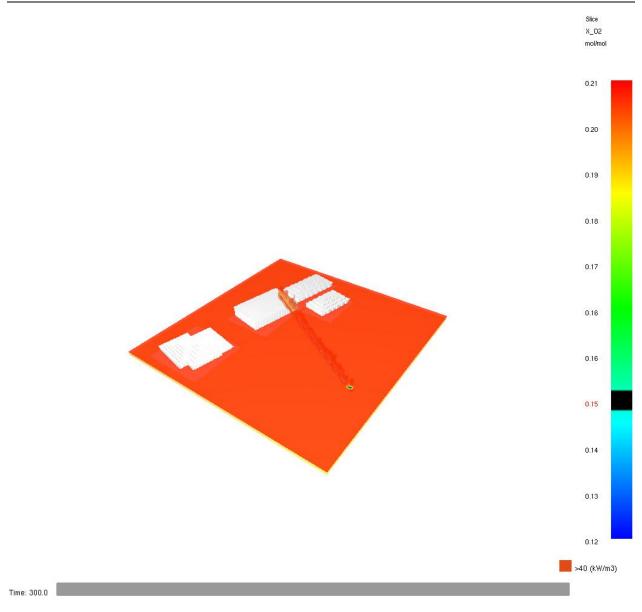


Figure 14: PFS-2 Wind, Z=2.0m, O2 at 300 seconds.

3.1.1.5. Temperature

The results indicating temperature (60°C maximum) are presented below by providing screen shots of the Smokeview visualization software output at multiple points in time during the fire development.

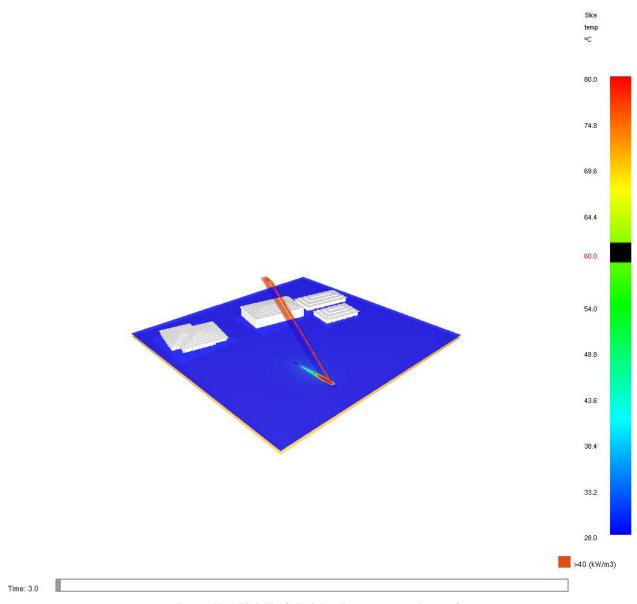


Figure 15: PFS-2 Wind, Z=2.0m, Temperature at 3 seconds.

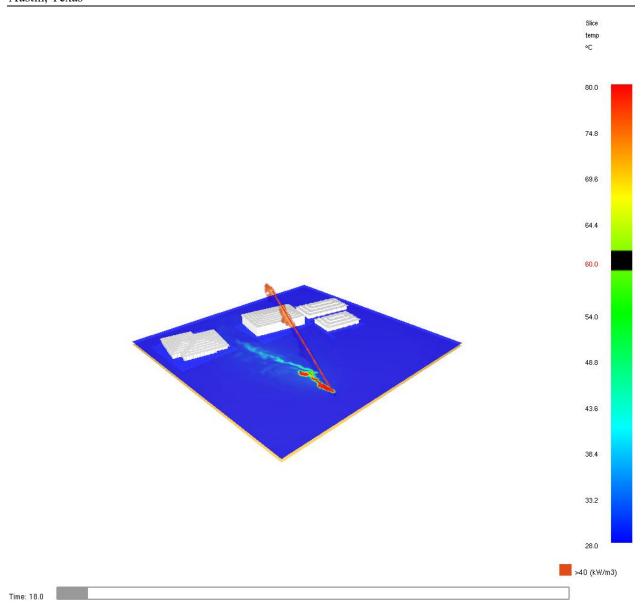


Figure 16: PFS-2 Wind, Z=2.0m, Temperature at 18 seconds.

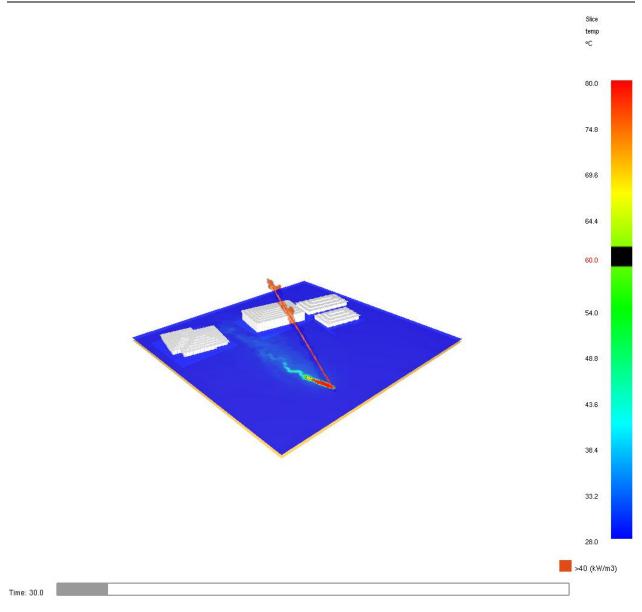


Figure 17: PFS-2 Wind, Z=2.0m, Temperature at 30 seconds.

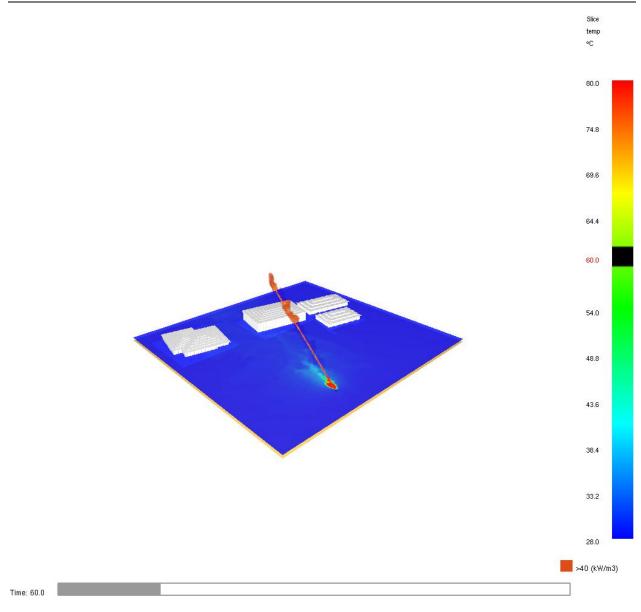


Figure 18: PFS-2 Wind, Z=2.0m, Temperature at 60 seconds.

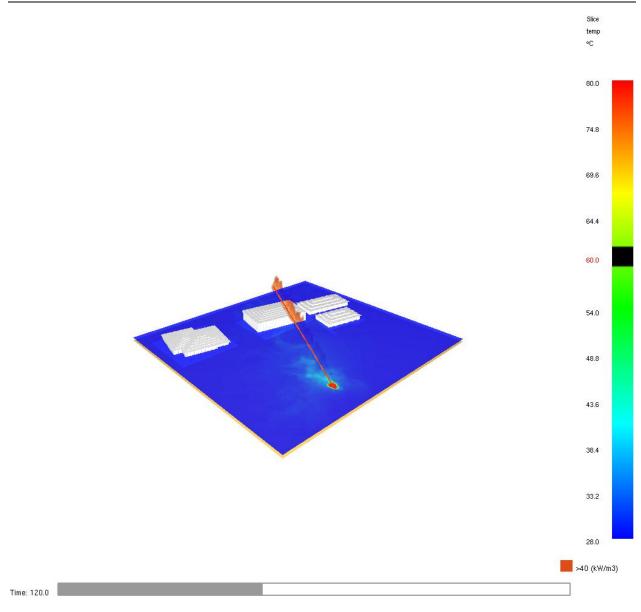


Figure 19: PFS-2 Wind, Z=2.0m, Temperature 120 seconds.

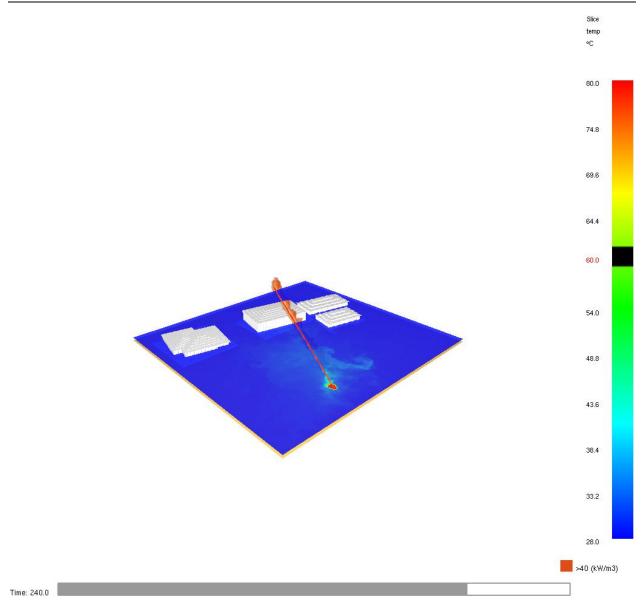


Figure 20: PFS-2 Wind, Z=2.0m, Temperature 240 seconds.

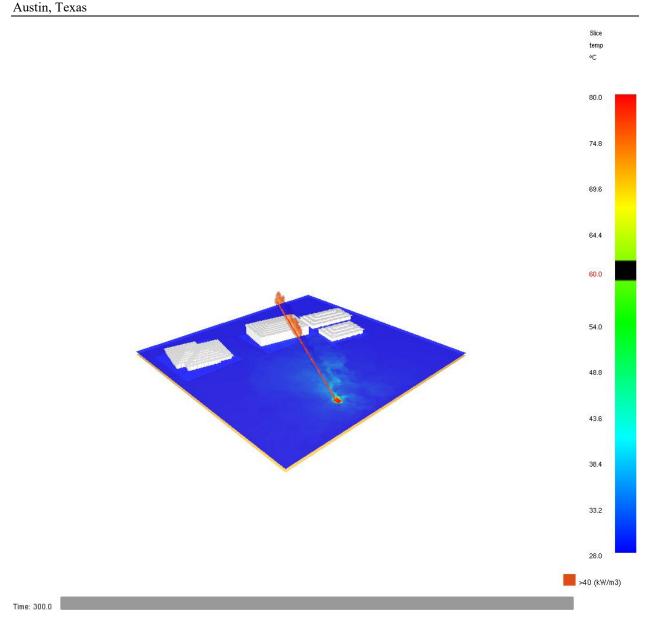


Figure 21: PFS-2 Wind, Z=2.0m, Temperature 300 seconds.

3.1.1.6. Visibility

Due to the clean-burning nature of propane, the results of the propane jet fire did not produce any soot or products that will limit or affect the visibility criteria.

4. Comparison of Results to Egress Time

The results of the modeling above show no signs of reaching the tenability threshold near the subject buildings at the equilibrium state; therefore, the tenability threshold will not ever be reached. Because of this, it can be stated that regardless of the time needed for egress, egress movement will not be challenged by the anticipated fire event. No further evaluation of egress time is needed.

January 29, 2018 Page 25 of 26

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

5. Conclusions

Building C is the closest building to the a hazardous pipeline, therefore additional fire modeling was performed, and reported in Appendix D which moved the fire in-line with the closest point of Building C. Upon evaluation of this fire model, the tenability limit for heat flux was found to be reached on the south face of Building C. For this reason, FPCG recommends that all egress paths from Building C be provided from the north-facing wall.

Based upon the proposed site development plan provided by your office, and upon review of the above reported results and attached in Appendix D, FPCG has concluded that the fire scenarios evaluated will permit adequate time for occupant evacuation to a safe place, as is required by Austin Code of Ordinance §25-2-516, Development Near A Hazardous Pipeline.

This concludes the Fire Modeling Report. If you have any questions, please contact me by phone at (210) 858-2389 or by e-mail at gilead@firepcg.com.

Sincerely yours,

Gilead R. Ziemba, P.E., M.Sc.

Tilead R. Ziemba

Partner & Sr. Fire Protection Engineer Fire Protection Consulting Group, LLC

Attachments: Appendix A - 17-065 - 31 Deerfield - Acceptance Criteria r2

Appendix B – 17-065 - 31 Deerfield - Hazard Analysis r1

Appendix C – Sample FDS Input File

Appendix D – 17-065 - CoA Comments on Fire Modeling Report FPCG Response r2

January 29, 2018 APPENDICES

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

Appendix A

17-065 - 31 Deerfield - Acceptance Criteria_r2

Via e-mail to: trac@practicerealestategroup.com



January 29, 2018

Mr. Trac Bledsoe Practice Real Estate Group 515 Congress, Suite 1515 Austin, Texas 78701

RE: Project Acceptance Criteria – Revision 2

31 Deerfield Tract Austin, Texas

Dear Mr. Bledsoe:

Thank you for contacting Fire Protection Consulting Group, LLC (FPCG) regarding this project. As part of the overall hazard analysis study and performance based design underway by FPCG, this report is being provided to gain acceptance of the proposed acceptance criteria to be used in the forthcoming evaluation of the 31 Deerfield Tract proposed Dialysis Clinic. FPCG requests that this report be provided to the Austin Fire Marshal's office for review, comments, and eventual approval so that this information can be utilized to develop the calculations or models that will be used to evaluate the acceptability of the new construction project. All values are based upon engineering judgement and research published in the SFPE Handbook of Fire Protection Engineering, 3rd Edition:

Purpose and Scope

The purpose of this report is to summarize the proposed acceptance criteria to be used to evaluate the hazard calculations and/or building fire models as part of the performance based analysis of the facility.

1. Proposed Required Safe Egress Time Criteria

The following are the proposed egress time criteria for the analysis.

1.1. Required Safe Egress Time (RSET)

The proposed minimum time for occupant evacuation to a safe place is either 1-hour or the maximum time required for safe evacuation when calculated by a Timed Egress Analysis, whichever is less.

2. Proposed Tenability Criteria

Tenability Criteria are utilized as part of egress system analysis. These criteria are used when determining the Available Safe Egress Time (ASET) and are compared to the Required Safe Egress Time (RSET) for acceptance. All tenability criteria will be evaluated at a point of six feet above the highest walking surface within the affected volume.

2.1. Heat Flux

The proposed heat flux tenability limit is 0.25W/cm² [2.5kW/m²] maximum. (SFPE Hbk, Figure 2-6.28)

2.2. Temperature

The proposed temperature tenability limit is 60°C [140°F] maximum. (SFPE Hbk, Figure 2-6.26)

2.3. Visibility

The proposed visibility tenability limit is 10 meters [32 feet] minimum. (SFPE Hbk, Table 2-6.10)

2.4. Carbon Dioxide Concentration

The proposed carbon dioxide concentration tenability limit is 40,000 parts-per million [4% by volume] maximum. (https://www.cdc.gov/niosh/idlh/124389.html)

2.5. Carbon Monoxide Concentration

The proposed carbon dioxide concentration tenability limit is 1200 parts-per million [0.0012% by volume] maximum. (https://www.cdc.gov/niosh/idlh/630080.html)

January 29, 2018 Page 3 of 2

Project Acceptance Criteria – Revision 2

31 Deerfield Tract

Austin, Texas

2.6. Oxygen Concentration

The proposed oxygen concentration tenability limit is 15% by volume minimum. (SFPE Hbk, Pg. 2-106)

If you have any questions, please contact me by phone at (210) 858-2389 or by e-mail at gilead@firepcg.com.

Sincerely yours,

Gilead R. Ziemba, P.E., M.

Partner & Sr. Fire Protection En

January 29, 2018 APPENDICES

Fire Modeling Report – Revision 2 31 Deerfield Tract

Austin, Texas

Appendix B

17-065 - 31 Deerfield - Hazard Analysis_r1

FIRE SCENARIO HAZARD ANALYSIS

Project Information:

31 Deerfield Tract Austin, Texas

Prepared For:

Practice Real Estate Group 515 Congress, Suite 1515 Austin, Texas 78701





339 Sandalwood Lane San Antonio, Texas 78216 www.FIREpcg.com Main Office +1 210.858.2389



Table of Contents

Pu	rpose a	and Scope	. 1
Lis	st of D	ocuments Reviewed	. 1
		ele Codes and Standards	
1.	Life	Safety Code Summary	. 2
2.	Haz	ard Analysis	. 4
	2.1.	Manual Fire Suppression	. 5
	2.2.	Magellan Crude Oil Pipeline	. 5
	2.2.1.	General Description	. 5
	2.2.2.	Project Fire Scenario #1 – Confined Crude Oil Pool Fire	. 5
	2.3.	Phillips 66 Liquified Propane Pipeline	. 5
	2.3.1.	General Description	. 5
	2.3.2.	Project Fire Scenario #2 – Propane Jet Fire	6
	2.4.	Kinder-Morgan Natural Gas Pipeline	. 7
	2.4.1.	General Description	. 7
	2.4.2.	Project Fire Scenario #3 – Natural Gas Jet Fire	. 7
	2.5	Conclusions and Recommendations for Modeling Scenarios	. 8





Table of Figures

Figure 1: Location of pipelines as reported by the Texas Railroad Commission (RRC) GIS mapping	4
Figure 2: Magellan pipeline data as reported by the RRC GIS mapping	5
Figure 3:Phillips pipeline data as reported by the RRC GIS mapping	
Figure 4: Austin annual wind rose. Source: www.tceq.texas.gov.	
Figure 5: PFS-2 heat release rate vs time.	
Figure 6:Kinder-Morgan pipeline data as reported by the RRC GIS mapping	
Figure 7: PFS-3 heat release rate vs. time	



Via e-mail to: trac@practicerealestategroup.com



September 8, 2017

Mr. Trac Bledsoe Practice Real Estate Group 515 Congress, Suite 1515 Austin, Texas 78701

RE: Fire Scenario Hazard Analysis – Revision 1

31 Deerfield Tract Austin, Texas

Dear Mr. Bledsoe:

Thank you for contacting Fire Protection Consulting Group, LLC (FPCG) regarding this project. As part of the overall performance based design planned to be provided by FPCG, this report is being provided to gain acceptance of several basis of design elements that are critical for to move forward with the analysis. FPCG requests that this report be provided to the Austin Fire Marshal's office for review, comments, and eventual approval so that this information can be utilized to develop the fire models that will be used to evaluate the Available Safe Egress Time for the facility and further substantiate the proposed developments compliance with the Austin Code of Ordinance §25-2-516, Development Near A Hazardous Pipeline.

Purpose and Scope

The purpose of this report is to summarize my evaluation of the fire hazard posed by the adjacent pipelines to this proposed development in Austin, Texas. This report addresses the follow topics:

• Hazard Analysis – FPCG has reviewed detailed information regarding the adjacent pipelines as well as the proposed development site plan. FPCG has developed a list of what we feel to be the worst-case fire scenarios. This section of the report summarizes our review, findings, and conclusions as to which fire scenarios should be evaluated via fire modeling as part of the overall performance based design.

The scope of this report is limited to these issues and only evaluates them based upon the information provided.

List of Documents Reviewed

The following is a list of documents received from your office that were reviewed or otherwise used in the preparation of this report:

- 31 Deerfield Grading & Utilities Exhibit.pdf
- GasLineLocMap.pdf

If any of these documents have changed from the version noted above, please contact our office to determine if the modification affects the results of this analysis and report.

Applicable Codes and Standards

The following codes and standards have been referenced and utilized during this analysis and form the basis for this report:

- Austin Code of Ordinance §25-2-516, Development Near A Hazardous Pipeline (ACO)
- 2012 edition of the International Building Code (IBC), as adopted by the City of Austin
- 2012 edition of the International Fire Code (IFC), as adopted by the City of Austin

Fire Scenario Hazard Analysis – Revision 1

31 Deerfield Tract

Austin, Texas

• 2012 edition of NFPA 101, Life Safety Code (LSC), as adopted by the Texas State Fire Marshal's Office

1. Life Safety Code Summary

The LSC provides guidance on selection of design fires in Chapter 5. The following is a summary of the requirements:

5.5*Design Fire Scenarios.

5.5.1 Approval of Parameters. The authority having jurisdiction shall approve the parameters involved in design fire scenarios. The proposed design shall be considered to meet the goals and objectives if it achieves the performance criteria for each required design fire scenario. (See 5.5.3.)

Resolution: FPCG is requesting review and approval of the design fire selected in the conclusions to this section of the report.

- **5.5.2* Evaluation.** Design fire scenarios shall be evaluated using a method acceptable to the authority having jurisdiction and appropriate for the conditions. Each design fire scenario shall be as challenging as any that could occur in the building, but shall be realistic, with respect to at least one of the following scenario specifications:
- (1) Initial fire location
- (2) Early rate of growth in fire severity
- (3) Smoke generation

Resolution: Each fire scenario listed in this report includes this information as part of the evaluation criteria.

- 5.5.3* Required Design Fire Scenarios. Design fire scenarios shall comply with the following:
- (1) Scenarios selected as design fire scenarios shall include, but shall not be limited to, those specified in 5.5.3.1 through 5.5.3.8.
- (2) Design fire scenarios demonstrated by the design team to the satisfaction of the authority having jurisdiction as inappropriate for the building use and conditions shall not be required to be evaluated fully.

Resolution: FPCG has noted beneath each Design Fire Scenario required by the LSC whether it is, in our opinion, appropriate or applicable to this evaluation. These notations are subject to review and approval by the AHJ.

- **5.5.3.1* Design Fire Scenario 1.** Design Fire Scenario 1 shall be described as follows:
- (1) It is an occupancy-specific fire representative of a typical fire for the occupancy.
- (2) It explicitly accounts for the following:
 - (a) Occupant activities
 - (b) Number and location of occupants
 - (c) Room size
 - (d) Contents and furnishings
 - (e) Fuel properties and ignition sources
 - (f) Ventilation conditions
 - (g) Identification of the first item ignited and its location

Resolution: This scenario is not applicable as the project does not involve a building fire.

5.5.3.2* Design Fire Scenario 2. Design Fire Scenario 2 shall be described as follows:

- (1) It is an ultrafast-developing fire, in the primary means of egress, with interior doors open at the start of the fire.
- (2) It addresses the concern regarding a reduction in the number of available means of egress.

Resolution: This scenario is represented in this analysis, though the fire location is exterior to the building. The intent is to determine if the fire scenarios will impede egress from the site.

5.5.3.3* Design Fire Scenario 3. Design Fire Scenario 3 shall be described as follows:

- (1) It is a fire that starts in a normally unoccupied room, potentially endangering a large number of occupants in a large room or other area.
- (2) It addresses the concern regarding a fire starting in a normally unoccupied room and migrating into the space that potentially holds the greatest number of occupants in the building.

Resolution: This scenario is not applicable as the project does not involve a building fire.

5.5.3.4* Design Fire Scenario 4. Design Fire Scenario 4 shall be described as follows:

- (1) It is a fire that originates in a concealed wall or ceiling space adjacent to a large occupied room.
- (2) It addresses the concern regarding a fire originating in a concealed space that does not have either a detection system or a suppression system and then spreading into the room within the building that potentially holds the greatest number of occupants.

Resolution: This scenario is not applicable as the project does not involve a building fire.

5.5.3.5* Design Fire Scenario 5. Design Fire Scenario 5 shall be described as follows:

- (1) It is a slowly developing fire, shielded from fire protection systems, in close proximity to a high occupancy area.
- (2) It addresses the concern regarding a relatively small ignition source causing a significant fire.

Resolution: Given the fuel source is flammable gasses, no "slow developing" fire scenario is used; however, the intent of this scenario is represented in this analysis as there is no automatic fire suppression anticipated. See Section 2 of this report.

5.5.3.6* Design Fire Scenario 6. Design Fire Scenario 6 shall be described as follows:

- (1) It is the most severe fire resulting from the largest possible fuel load characteristic of the normal operation of the building.
- (2) It addresses the concern regarding a rapidly developing fire with occupants present.

Resolution: This scenario is represented in this analysis. See Section 2 of this report.

5.5.3.7* Design Fire Scenario 7. Design Fire Scenario 7 shall be described as follows:

- (1) It is an outside exposure fire.
- (2) It addresses the concern regarding a fire starting at a location remote from the area of concern and either spreading into the area, blocking escape from the area, or developing untenable conditions within the area.

Resolution: This scenario is represented in this analysis. See Section 2 of this report.

5.5.3.8* Design Fire Scenario 8. Design Fire Scenario 8 shall be described as follows:

(1) It is a fire originating in ordinary combustibles in a room or area with each passive or active fire protection system independently rendered ineffective.

- (2) It addresses concerns regarding the unreliability or unavailability of each fire protection system or fire protection feature, considered individually.
- (3)*It is not required to be applied to fire protection systems for which both the level of reliability and the design performance in the absence of the system are acceptable to the authority having jurisdiction.

Resolution: This scenario is not applicable as the project does not involve a building fire.

5.5.4 Design Fire Scenarios Data.

- 5.5.4.1 Each design fire scenario used in the performance based design proposal shall be translated into input data specifications, as appropriate for the calculation method or model.
- 5.5.4.2 Any design fire scenario specifications that the design analyses do not explicitly address or incorporate and that are, therefore, omitted from input data specifications shall be identified, and a sensitivity analysis of the consequences of that omission shall be performed.
- 5.5.4.3 Any design fire scenario specifications modified in input data specifications, because of limitations in test methods or other data-generation procedures, shall be identified, and a sensitivity analysis of the consequences of the modification shall be performed.

Resolution: The hazard analysis section of this report addresses these issues.

For clarity, each LSC Fire Scenario noted above will be referred to in this report as "LSCFS" followed by the number described above. For example, LSCFS-1 refers to the Life-Safety Code Fire Scenario 1, and so-on.

2. Hazard Analysis

Given the purpose of this report, this hazard analysis will focus on a potential release of material from a pipeline that could result in a large, sustained fire event thereby putting occupants in danger of being overcome by the fire or products of combustion. Upon review of the documents provided by your office, the following hazards have been identified and quantified in terms of intensity and duration to select the worst-case fire scenarios as the design fire for the overall performance-based egress analysis. Please refer to Appendix A of this report for a diagram depicting the location and identification of each Project Fire Scenario described in detail below. For clarity, each Project Fire Scenario described below will be referred to in this report as "PFS" followed by the number associated with that scenario. For example, PFS-1 refers to the Project Fire Scenario 1 described below and located in Appendix A.

This analysis evaluates potential sustained fire scenarios from three adjacent pipelines. Explosion scenarios are not part of this analysis as the ACO does not request evaluation of explosions for compliance with the Ordinance.

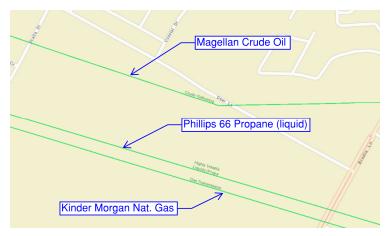


Figure 1: Location of pipelines as reported by the Texas Railroad Commission (RRC) GIS mapping.

2.1. Manual Fire Suppression

Manual fire suppression response from dedicated, trained personnel is not considered as part of this evaluation.

2.2. Magellan Crude Oil Pipeline

The following is a summary of FPCG's assessment and the most likely fire scenario associated with crude oil pipeline.

2.2.1.General Description

The following information is known about said pipeline:

GIS Identify Results - Pipeline Attributes

COUNTY_FIPS	453				
OPERATOR	MAGELLAN PIPELINE COMPANY, L.P.				
COMMODITY	CRUDE OIL				
COMMODITY DESCRIPTION	CRUDE OIL				
SYSTEM TYPE	Crude Gathering				
SYSTEM NAME	LONGHORN				
DIAMETER	18				
T4PERMIT	05431				
T4PERMIT MILES	11.04000000000001				
STATUS	In Service				
INTERSTATE	Yes				

Figure 2: Magellan pipeline data as reported by the RRC GIS mapping.

2.2.2. Project Fire Scenario #1 – Confined Crude Oil Pool Fire

Upon further review of the site building locations with respect to the crude oil pipeline, all proposed buildings will be located further than 500 feet away from said pipeline. For this reason, PFS-1 has been eliminated from the analysis as the Hazardous Pipeline Ordinance exempts buildings over 500 feet away from requiring evaluation.

2.3. Phillips 66 Liquified Propane Pipeline

The following is a summary of FPCG's assessment and the most likely fire scenario associated with the propane pipeline.

2.3.1.General Description

The following information is known about said pipeline:

GIS Identify Results - Pipeline Attributes

COUNTY_FIPS	453
OPERATOR	PHILLIPS 66 PIPELINE LLC
COMMODITY	NATURAL GAS LIQUIDS
COMMODITY DESCRIPTION	NATURAL GAS LIQUIDS
SYSTEM TYPE	Highly Volatile Liquids (Propa
SYSTEM NAME	BENEDUM TO SWEENY
SUBSYSTEM NAME	BENEDUM/SWEENY
DIAMETER	10.75
T4PERMIT	05997
T4PERMIT MILES	27.34
STATUS	In Service
INTERSTATE	Yes

Figure 3:Phillips pipeline data as reported by the RRC GIS mapping

2.3.2. Project Fire Scenario #2 – Propane Jet Fire

FPCG anticipates that a release of liquified propane will result in a highly buoyant vapor cloud formation, therefore would result in an explosion or fire ball rather than a sustained fire event. As explosion scenarios are excluded from this evaluation, FPCG will evaluate the likely sustained fire event following an explosion or fire ball event, which would be an ignited pressurized plume release of propane resulting in a very strong jet fire.

This fire scenario can be considered to represent LSCFS-6 or -7. Because this fire is and exterior fire exposure hazard in an area with no suppression system, and is anticipated to cause some delay or disruption to building evacuation, this fire scenario can also be considered to represent LSCFS-1, -2, -5 and -7. The constants, fuel properties, and assumptions included as part of this PFS are as follows:

- The jet diameter is that of the open end of the pipeline, or 10.75 inches.
- The open pipe, after rupturing from an explosion, is pointing directly up and is not impeded by the soil as it reaches the atmosphere.
- As the jet flame, when pointing upward, could not impinge directly on any structure, the radiative mode of heat transfer will govern as the greatest hazard. As the cross-wind condition could deflect the jet flame closer to the development, increasing radiative heat flux to the development, the cross-wind flame length is used.
- The highest wind velocity expected is 20 knots. See annual wind rose for the Austin area provided in Figure 4.
- The pipeline operating pressure is 1200psi.¹
- The orifice K-factor is 1.55 for an open, splayed pipe end that could result from an explosion.
- Liquified propane will turn to gas nearly instantaneously at atmospheric pressure.
- The propane has a heat of combustion of 46.3 kJ/g.
- The fuel source is effectively unlimited, therefore there is no growth or decay period.

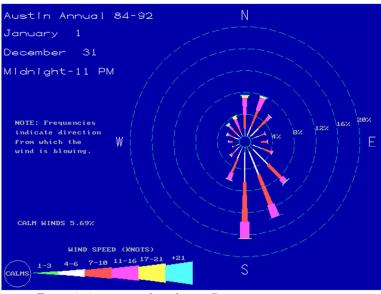


Figure 4: Austin annual wind rose. Source: www.tceq.texas.gov.

Based upon these factors noted above, FPCG has developed the following heat release rate (HRR) curve depicting the HRR over time for PFS-2 which is depicted in Figure 5 below. Full spreadsheet calculation data is provided in Appendix B.

¹ Alzbutas, R. et. al; "Risk and Uncertainty Analysis of Gas Pipeline Failure and Gas Combustion Consequence". Springer-Verlag; Berlin Heidelberg. 2014.

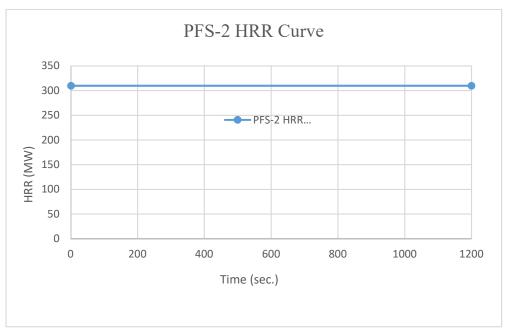


Figure 5: PFS-2 heat release rate vs time.

2.4. Kinder-Morgan Natural Gas Pipeline

The following is a summary of FPCG's assessment and the most likely fire scenario associated with the natural gas pipeline.

2.4.1. General Description

The following information is known about said pipeline:

GIS Identify Results - Pipeline Attributes

COUNTY_FIPS	453
OPERATOR	KINDER MORGAN TEXAS PIPELINE LLC
COMMODITY	NATURAL GAS
COMMODITY DESCRIPTION	NATURAL GAS
SYSTEM TYPE	Gas Transmission
SYSTEM NAME	HILL COUNTRY PIPELINE (RANCHO)
SUBSYSTEM NAME	LCRA TO GARFIELD STA.
DIAMETER	24
T4PERMIT	00762
T4PERMIT MILES	27.38
STATUS	In Service
INTERSTATE	No

Figure 6:Kinder-Morgan pipeline data as reported by the RRC GIS mapping

2.4.2. Project Fire Scenario #3 – Natural Gas Jet Fire

FPCG anticipates that a release of natural gas will result in a highly buoyant vapor cloud formation, therefore would result in an explosion or fire ball rather than a sustained fire event. As explosion scenarios are excluded from this evaluation, FPCG will evaluate the likely sustained fire event following an explosion or fire ball event, which would be an ignited pressurized plume release of natural gas resulting in a very strong jet fire.

This fire scenario can be considered to represent LSCFS-6 or -7. Because this fire is and exterior fire exposure hazard in an area with no suppression system, and is anticipated to cause some delay or disruption

to building evacuation, this fire scenario can also be considered to represent LSCFS-1, -2, -5 and -7. The constants, fuel properties, and assumptions included as part of this PFS are as follows:

- The jet diameter is that of the open end of the pipeline, or 24 inches.
- The open pipe, after rupturing from an explosion, is pointing directly up and is not impeded by the soil as it reaches the atmosphere.
- As the jet flame, when pointing upward, could not impinge directly on any structure, the radiative mode of heat transfer will govern as the greatest hazard. As the cross-wind condition could deflect the jet flame closer to the development, increasing radiative heat flux to the development, the crosswind flame length is used.
- The highest wind velocity expected is 20 knots. See annual wind rose for the Austin area provided in Figure 4.
- The pipeline operating pressure is 1200psi.²
- The orifice K-factor is 1.55 for an open, splayed pipe end that could result from an explosion.
- The natural gas has a heat of combustion is similar to that of methane and is 50.0 kJ/g.
- The thermo-physical properties of the natural gas are similar to that of methane for all engineering constants.
- The fuel source is effectively unlimited, therefore there is no growth or decay period.

Based upon these factors noted above, FPCG has developed the following heat release rate (HRR) curve depicting the HRR over time for PFS-3 which is depicted in Figure 7 below. Full spreadsheet calculation data is provided in Appendix B.

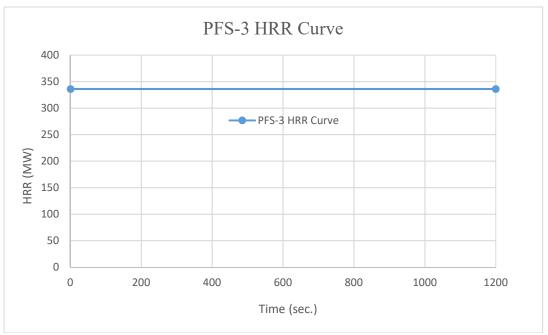


Figure 7: PFS-3 heat release rate vs. time.

2.5. Conclusions and Recommendations for Modeling Scenarios

Based upon the information provided by your office, and upon the evaluation summarized above, FPCG recommends proceeding to the modeling stage of the project for only the following Project Fire Scenarios:

² Alzbutas, R. et. al; "Risk and Uncertainty Analysis of Gas Pipeline Failure and Gas Combustion Consequence". Springer-Verlag; Berlin Heidelberg. 2014.

Austin, Texas

• PFS-2: Phillips 66 Liquified Propane Pipeline Jet Fire. This scenario represents a larger radiative energy output than that of PFS-1 or PFS-3. FPCG's calculations anticipate flame length over 70 meters long, which will extend towards the development in a cross-wind condition. Though very similar to PFS-3, propane has three times the amount of carbon atoms per mole, and will therefore produce significantly more radiative energy, which is the expected worst-case heat transfer mode for jet flames that do not impinge on a target. For these reasons, FPCG has included this scenario for further evaluation.

The following Project Fire Scenarios are to be eliminated from further analysis:

- PFS-1: Magellan Crude Oil Pipeline Confined Pool Fire. This pipeline has been determined to be further than 500 feet to the closest building on-site, therefore, this pipeline is not required to be evaluated per the Hazardous Materials Pipeline Ordinance.
- PFS-3: Kinder Morgan Natural Gas Pipeline Jet Fire. As this fire is very similar is HRR to that of PFS-2, is further from the development, and is expected to produce about half of the radiative energy than the PFS-2 fire, FPCG has eliminated this scenario from further evaluation.

This concludes the Fire Scenario Hazard Analysis. If you have any questions, please contact me by phone at (210) 858-2389 or by e-mail at gilead@firepcg.com.

Sincerely yours,

Gilead R. Ziemba, P.E., M.Sc.

Partner & Sr. Fire Protection Engine

Attachments: Appendix A – Fire Scenario Location Drawing r1

Appendix B – Fire Scenario Calculations

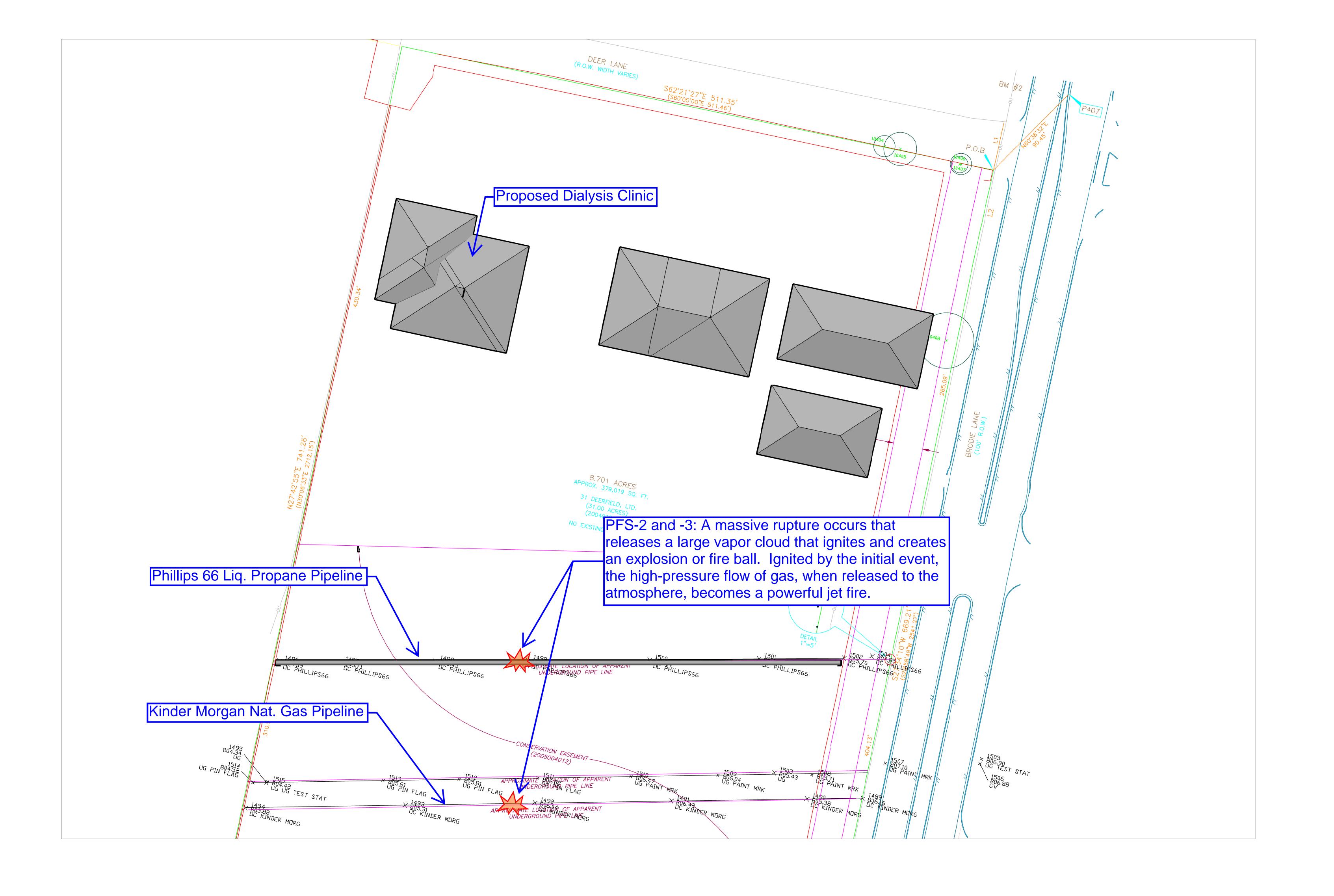
September 8, 2017 APPENDICES

Fire Scenario Hazard Analysis – Revision 1

31 Deerfield Tract
Austin, Texas

Appendix A

Fire Scenario Location Drawing_r1



September 8, 2017	APPENDICES
Fire Scenario Hazard Analysis – Revision 1	

31 Deerfield Tract Austin, Texas

Appendix B

Fire Scenario Calculations

PFS-2 Propane Jet Fire

339 Sandalwood Lane San Antonio, Texas 78216 Main Office +1 210.858.2389 www.FIREpcg.com

Momentum Controlled Regime

See Beyler - SFPE Hbk. 5th Edition, Chapter 66, Pages 2631-2645, Eq. 66.37 and 66.38

 $dj (in) \\ \qquad \qquad CT (Table 66.12) \\ \qquad \qquad Ma (g/mol) \\ \qquad \qquad Mf (g/mol)$

10.75 0.27305 0.038 29 44.1

Lf (m) Q (MW)

87.40364562 439.15

Buoyancy Controlled Regime

See Beyler - SFPE Hbk. 5th Edition, Chapter 66, Pages 2631-2645, Eq. 66.37 and 66.38

dj (in) dj (m) CL (lean flammability limit) g (m/sec^2) Uj (m/sec) Ca (kJ/kg) Ta (Rankine) ΔHc (kJ/g)

10.75 0.27305 0.021 9.81 422 1 565 46.3

Lf (m) Q (MW)

257.0849617 1632.72

Calculate Flame Length with Cross-Wind Condition

Wind Velocity (knots) Wind Velocity (ft/sec.) uw (m/sec.) uj/uw CL-bar SL-bar XL-bar ZL-bar

20 33.8000 10.30224 40.9620 1.308 2.2912 0.6412 1.801333903

Propane Density (kg/m^3) Ambient Air Density (kg/m^3) X (m) Z (m)

1.88 1.205 8.958243319 25.16532787

R (Uw/Uj) α (degrees) Ds L-BV (m) Q (MW)

0.024412891 48.20945116 0.42600332 65.6823817 309.87

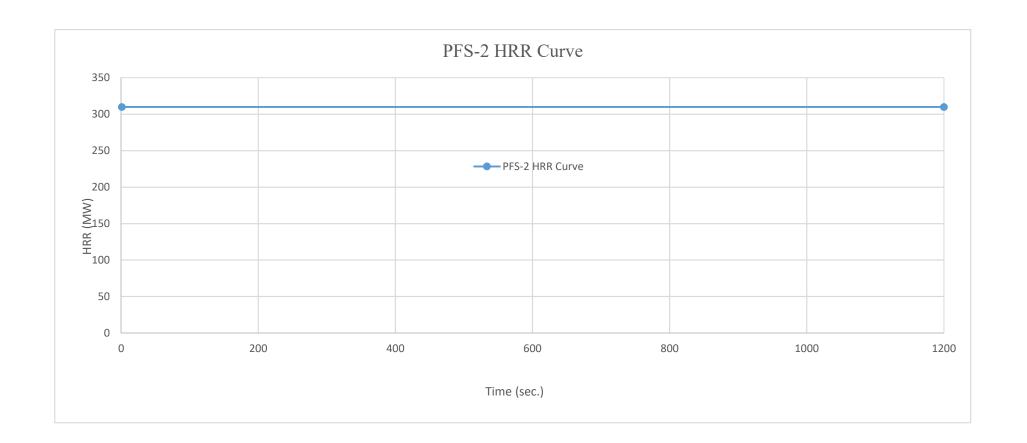
t (sec) PFS-2 HRR Curve

1 310

1200 310

PFS-2 Propane Jet Fire





PFS-3 Natural Gas Jet Fire

339 Sandalwood Lane San Antonio, Texas 78216 Main Office +1 210.858.2389 www.FIREpcg.com

Momentum Controlled Regime

See Beyler - SFPE Hbk. 5th Edition, Chapter 66, Pages 2631-2645, Eq. 66.37 and 66.38

 $dj (in) \\ \qquad \qquad CT (Table 66.12) \\ \qquad \qquad Ma (g/mol) \\ \qquad \qquad Mf (g/mol)$

24 0.6096 0.091 29 16

Lf (m) Q (MW)

135.2800742 747.71

Buoyancy Controlled Regime

See Beyler - SFPE Hbk. 5th Edition, Chapter 66, Pages 2631-2645, Eq. 66.37 and 66.38

dj (in) dj (m) CL (lean flammability limit) g (m/sec^2) Uj (m/sec) Ca (kJ/kg) Ta (Rankine) ΔHc (kJ/g)

24 0.6096 0.05 9.81 422 1 565 50.0

Lf (m) Q (MW)

286.0162226 1858.68

Calculate Flame Length with Cross-Wind Condition

Wind Velocity (knots) Wind Velocity (ft/sec.) uw (m/sec.) uj/uw CL-bar SL-bar XL-bar ZL-bar

20 33.8000 10.30224 40.9620 1.130 2.5107 0.8607 1.956103928

Nat Gas Density (kg/m^3) Ambient Air Density (kg/m^3) X (m) Z (m)

0.9 1.205 18.57448999 42.21292078

R (Uw/Uj) α (degrees) Ds L-BV (m) Q (MW)

0.024412891 48.20945116 0.455302905 70.19987356 336.09

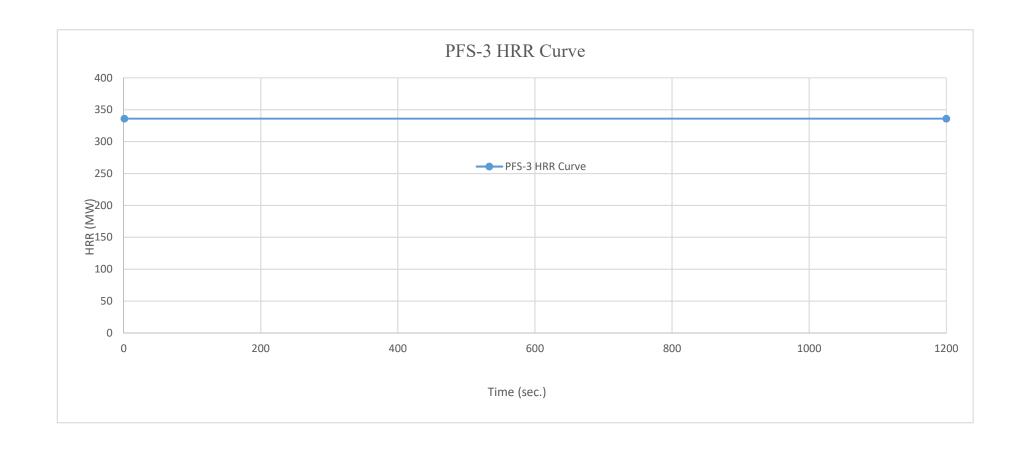
t (sec) PFS-3 HRR Curve

1 336

1200 336

PFS-3 Natural Gas Jet Fire







PFS-2 and -3 Fuel Velocity

PFS-2: Gas Release Velocity

Rupture Diam. (in)	Area of Rupture (in^2)		Area of Rupture (ft^2)	Gas Flow (ft^3/sec)		
	10.75		90.7626	0.6303	412.	5
Gas Pressure (psi)		Gas Head (ft)		Gas Velocity (ft/sec.)	Gas Velocity (m/sec.)	Orifice K-factor
	1200		2771.3626	422.2027	128.687393	9 1.55
Wind Velocity (knots)		Wind Velocity (ft/sec.)		U/Uj		
	20		33.8000	0.0801		
Propane Density (kg/m	^3)	Ambient Air Density (k	g/m^3)			
	1.88		1.205			

PFS-3: Gas Release Velocity

		113 3. 0	as itelease velocity		
Rupture Diam. (in)	Area of Rupture (in	^2) Area of Ruptu	re (ft^2) Gas Flo	w (ft^3/sec)	
	24	452.3893	3.1416	2055.9	
as Pressure (psi)	Gas Head (ft)	Gas Velocity (ft/sec.) Gas Vel	ocity (m/sec.) Orifi	ice K-factor
	1200	2771.3626	422.2027	128.6873939	1.55
nd Velocity (knots)	Wind Velocity (ft/s	ec.) U/Uj			
	20	33.8000	0.0801		
at Gas Density (kg/m ^a	3) Ambient Air Densit	y (kg/m^3)			
	0.9	1.205			

January 29, 2018 APPENDICES

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

Appendix C

Sample FDS Input File

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```
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JetFire 32 N C3H8.fds

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JetFire 32 N C3H8.fds

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JetFire_32_N_C3H8.fds

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&OBST ID='Professional Office Building C', XB=119.5,121.5,69.0,69.5,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=122.0,123.5,68.5,69.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=124.0,126.0,68.0,68.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=126.5,128.5,67.5,68.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=129.0,130.5,67.0,67.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=131.0,133.0,66.5,67.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=133.5,134.5,66.0,66.5,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=134.5,135.0,67.5,69.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=135.0,135.5,69.5,71.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=135.5,136.0,72.0,73.5,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=136.0,136.5,74.5,76.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=136.5,137.0,76.5,78.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=137.0,137.5,79.0,80.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=128.5,128.5,75.0,75.5,7.0,7.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=131.0,131.0,71.5,72.0,6.0,6.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=133.0,133.0,68.0,68.5,5.0,5.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,110.5,82.0,84.5,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,110.5,88.0,89.0,4.5,5.0, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,111.0,84.5,87.0,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,111.5,87.0,87.5,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,111.5,80.0,82.0,0.0,5.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.0,116.0,87.5,88.0,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.5,111.5,88.5,89.0,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=110.5,112.0,82.0,84.5,0.0,5.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/

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&OBST ID='Professional Office Building C', XB=112.5,114.5,88.5,89.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=113.5,152.5,88.0,88.5,0.0,0.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=115.0,116.5,88.0,88.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=117.0,119.0,87.5,88.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=119.5,121.5,87.0,87.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=122.0,123.5,86.5,87.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=124.0,126.0,86.0,86.5,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=126.5,128.5,85.5,86.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=129.0,130.5,85.0,85.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=131.0,133.0,84.5,85.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=133.5,135.5,84.0,84.5,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=136.0,137.5,83.5,84.0,4.5,4.5, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=137.0,137.5,80.0,81.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=137.5,138.0,81.5,83.0,4.5,4.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=117.0,118.0,80.0,80.0,7.0,7.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=124.0,125.0,80.0,80.0,6.5,7.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=131.0,132.5,80.0,80.0,6.0,6.5, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building C', XB=134.0,134.5,81.0,81.0,5.5,6.0, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building C', XB=111.5,152.5,110.0,116.0,0.0,0.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building D', XB=105.5,110.0,65.0,80.0,0.0,0.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building D', XB=105.5,110.0,80.0,90.0,0.0,0.0, COLOR='WHITE', PERMIT HOLE=.FALSE., ALLOW VENT=.FALSE., SURF ID='Global'/ &OBST ID='Professional Office Building D', XB=110.0,139.5,65.0,80.0,0.0,0.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building D', XB=112.0,112.5,97.5,98.5,4.5,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/ &OBST ID='Professional Office Building D', XB=112.0,118.0,97.0,97.5,0.0,5.0, COLOR='WHITE', PERMIT_HOLE=.FALSE., ALLOW_VENT=.FALSE., SURF_ID='Global'/

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JetFire 32 N C3H8.fds
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JetFire_32_N_C3H8.fds
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JetFire 32 N C3H8.fds
XB=110.0,160.0,0.0,40.0,80.0,80.0, COLOR='INVISIBLE'/
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&SLCF QUANTITY='TEMPERATURE', VECTOR=.TRUE., PBZ=0.0/
```

&TAIL /

Page 82

January 29, 2018 APPENDICES

Fire Modeling Report – Revision 2 31 Deerfield Tract Austin, Texas

Appendix D

17-065 CoA Comments on Fire Modeling Report_FPCG Response_r2





January 29, 2018

Ms. Corazon Urgena, P.E. Austin Fire Department Emergency Prevention Division 505 Barton Springs Road, Suite 200 Austin, TX 78704 Via E-mail to: cora.urgena@austintexas.gov

RE: Review Comments for Fire Modeling Report – Revision 2

31 Deerfield Tract Deer Lane and Brodie Lane Austin, Texas

Ms. Urgena,

Here are the responses to your comments returned via e-mail dated October 6, 2017. Please let me know if you have any further questions.

1. Can distances and heights from the source be shown for the tenability limits of heat flux, temperature, etc.?

Yes. In order not to keep the fire modeling report as short as possible, the following links have been provided to several folders containing screen shots with a grid (units in meters) for the project acceptance criteria.

Jet Fire – Building C Aligned:

• Net Heat Flux https://www.dropbox.com/sh/6j3h9bxlwuko1h9/AAApFS1oQZycD5sbGYxiYmBTa?dl=0

Jet Fire - South:

- Net Heat Flux https://www.dropbox.com/sh/8j2o0rzi87dyrby/AACbkTeI oDqb-G3z-TxpNAfa?dl=0
- Temperature https://www.dropbox.com/sh/ywtgs27nrxx7zui/AABt3RA3uq0KTJe1dS zT3doa?dl=0
- Oxygen

https://www.dropbox.com/sh/bvkveo0umvs1ok1/AACfK6j0-bXIVxttd2OVksYva?dl=0

- Carbon Dioxide https://www.dropbox.com/sh/g7psnzm9cmjo2mi/AADjDLgzIyzZ7F-cT1wVCUYfa?dl=0
- Carbon Monoxide https://www.dropbox.com/sh/dvdpb1qzfcyra5h/AAB8WRct7UdhjxvrHKX Eiuda?dl=0

Jet Fire - North:

- Net Heat Flux
 - https://www.dropbox.com/sh/i5309604a9f77vt/AADZXoxatlGwWK-f9CO7tZ3ga?dl=0
- **Temperature** https://www.dropbox.com/sh/lgvic62tq3had3m/AAAF8V9URMrQXZzZ-XFU5k_ha?dl=0
- Oxygen https://www.dropbox.com/sh/n9vqeu2d7fohafl/AAA0-S7CQAXVmwQ3UdvGRqzda?dl=0
- Carbon Dioxide https://www.dropbox.com/sh/djsft3p0obtgt0a/AAB9T3fCgbRNVSB8TtsKkgvAa?dl=0

January 29, 2018 Page 2 of 3

Review Comments for Fire Modeling Report – Revision 2 31 Deerfield Tract

Deer Lane and Brodie Lane

Austin, Texas

Carbon Monoxide
 https://www.dropbox.com/sh/zhlwsn9n763yngz/AAAOIzMg9_tnlUJrUYnVA1lGa?dl=0

2. Verify if Part (B) (1) Sections (b) through (j) of the Pipeline Ordinance will be addressed in a separate report.

Confirmed. FPCG has provided a separate letter to address items (b) through (j).

3. Verify if a system for early detection and notification of a pipeline leak will be addressed in a separate report.

FPCG has attached the system design drawings to the letter describing how each of the section of the Hazardous Pipeline Ordinance are addressed. Please see said letter for the design.

4. An additional explanation/description of the results may be needed for Council members and their staff.

Understood. Additional information will be provided, as needed. FPCG anticipates a presentation to Council to allow an opportunity to field questions.

5. The report is being reviewed by other AFD staff members. Additional comments may be forthcoming

Understood.

Additional comments were provided by you via e-mail dated October 18, 2017.

1. Provide an executive summary [to the Fire Modeling Report].

A revised Fire Modeling Report has been provided with an executive summary.

2. Chuck Lesniak questioned the orientation of the jet fire pointing straight up. Provide a justification.

The jet fire is modeled at the angle specified in the hazard analysis. Please see additional screen shots for clarification.

3. The early detection and notification system design must address how occupants will be notified to evacuate the building. AFD is also concerned about the migration of flammable gases from an underground release into the buildings. This may require gas detection devices inside the buildings on the first level.

FPCG has modified the detection and alarm system design based upon AFD comments.

4. AFD may require a fire barrier wall at the property line. This decision will be made once we receive all the information requested.

FPCG feels that the fire modeling report indicates that the worst-case fire does not threaten the development in a way that justifies additional construction measures beyond the recommendations provided by FPCG in the Conclusions of the Fire Modeling Report, Revision 2.

January 29, 2018 Page 3 of 3

Review Comments for Fire Modeling Report – Revision 2

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31 Deerfield Tract

Deer Lane and Brodie Lane

Austin, Texas

If you have any questions, please do not hesitate to contact me by phone at (210) 858-2389 or by e-mail to

gilead@firepcg.com.

Sincerely yours,

Gilead R. Ziemba, P.E., M.Sc.

Partner & Sr. Fire Protection Engineer